

MACHINE TOOL

Tool Geometry

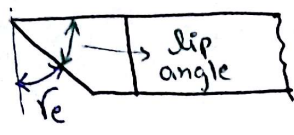
C_s = Side cutting edge
 C_e = end cutting edge

Top view of single point cutting tool

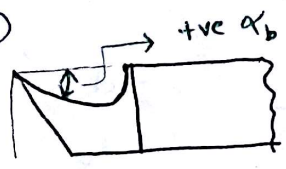
Tool life

15-30° C_s

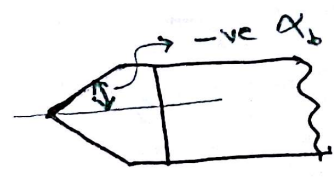
• Back rake angle (α_b)



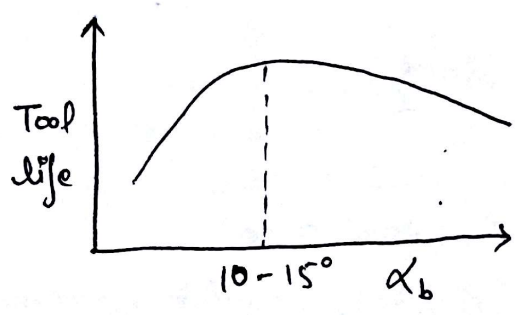
- used for medium strength w/p
- C.I, Brass



- used for Soft & Ductile w/p
- M.S.



- Used for hard & Brittle w/p
- Carbide



LATHE

• Cutting velocity = $v = \frac{\pi D N}{1000}$

here, $v = \text{m/min}$
 $D = \text{mm}$
 $N = \text{rpm}$

• machining time = $t_m = \frac{L_c}{f N}$

here $L_c = \text{mm}$
 $f = \text{mm/rev}$
 $N = \text{rpm}$
 $t_m = \text{min}$

• $MRR = f d v \times 1000 = \frac{\text{mm}^3}{\text{min}}$

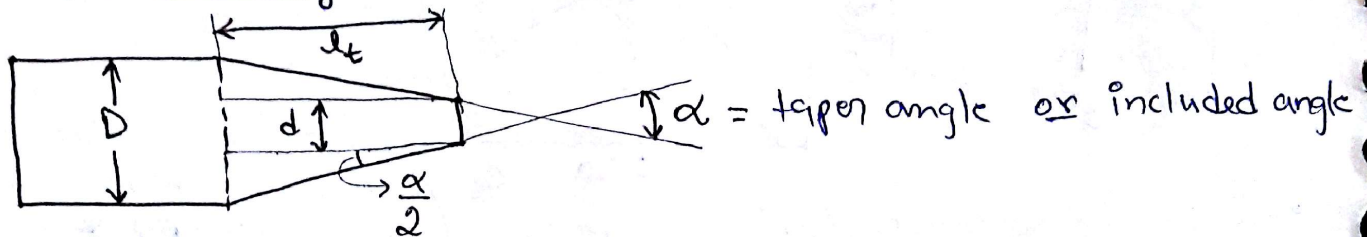
$\swarrow$ $\downarrow$ $\searrow$
 $\frac{\text{mm}}{\text{rev}}$ mm m/min

- Speed ratio in automobile & m/c tools generally follows geometric progression

$$N_{\max} = N_{\min} \gamma^{n-1}$$

$$\frac{N_{\max}}{N_{\min}} = \gamma^{n-1} = \text{Speed range ratio} = \frac{V_{\max} \cdot D_{\max}}{V_{\min} \cdot D_{\min}}$$

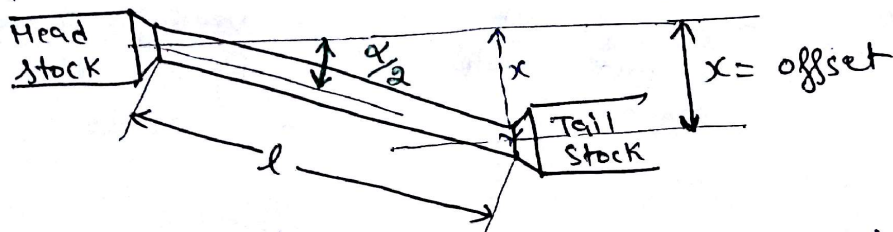
• Taper turning



$$\Rightarrow \tan\left(\frac{\alpha}{2}\right) = \frac{D-d}{2 \times l_t}$$

here, l_t = taper length

$\Rightarrow$ In tail stock offset method



$$\sin\left(\frac{\alpha}{2}\right) = \frac{x}{l} \Rightarrow x = l \sin\left(\frac{\alpha}{2}\right)$$

• Turret lathe

- Rigid m/c, hold workpiece upto 200 mm (Turret mounted on saddle).
- no restriction on turret travel
- feed is slow
- No tail stock,
- 2 tool post $\Rightarrow$ 4 turning tool
- 1 turret $\Rightarrow$ only grinding tool

Capstan lathe

- less rigidity (turret is mounted on auxiliary slides), small jobs upto 60 mm
- Auxiliary slides limit the travel distance
- feed is fast
- No tail stock
- 2 tool post $\Rightarrow$ 4 turning tool
- 1 turret $\Rightarrow$ only grinding tool

- when doing milling on lathe m/c, milling cutter is fixed in chuck.

- For metric threads, thread angle = 60°
- most used threads



ACME

- Bear load in both dirⁿ
- lead screw



Butress

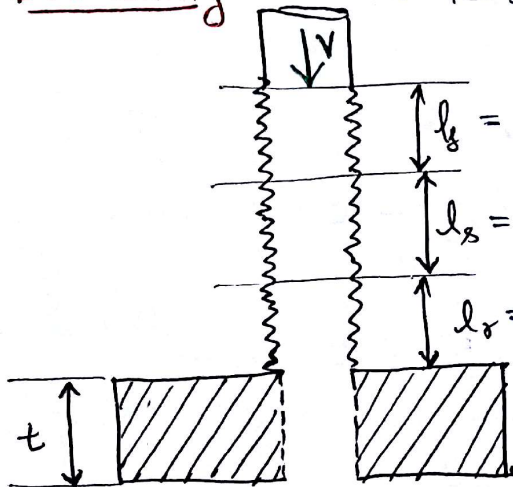
- Bear load in 1 dirⁿ
- Bench vice

- Thread cutting on lathe [thread churning] ^(Swiss automatic) [High Quality threads]
- ⇒ RHT ⇒ move $R \rightarrow L$ [odd no. of idlers used]
- ⇒ LHT ⇒ move $L \rightarrow R$ [even no. of idlers used]
- Gear ratio = train value = Transformation ratio

$$= \frac{\text{lead of workpiece}}{\text{lead of lead screw}} \quad [\because \text{for thread cutting}]$$
- ⇒ 127 teeth gear is called translating gear and is used to convert pitch from inches to mm from lead screw to w/p.

Broaching

- least cutting speed



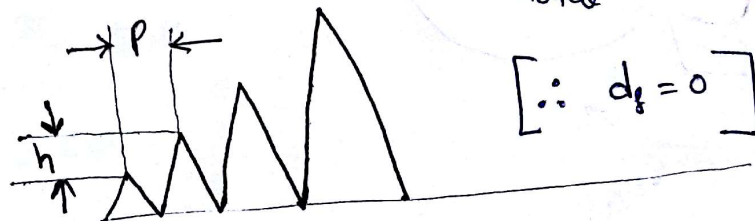
$$l_f = \text{length of finishing teeth} = n_f \cdot P_f \Rightarrow n_f \cdot P_f$$

$$l_s = \text{length of semi-finishing teeth} = n_s \cdot P_s = \frac{d_s}{h_s} \cdot P_s$$

$$l_r = \text{length of roughing teeth} = n_r \cdot P_r = \frac{d_r}{h_r} \cdot P_r$$

$$d_{\text{total}} = d_r + d_s$$

$$[\because d_f = 0]$$



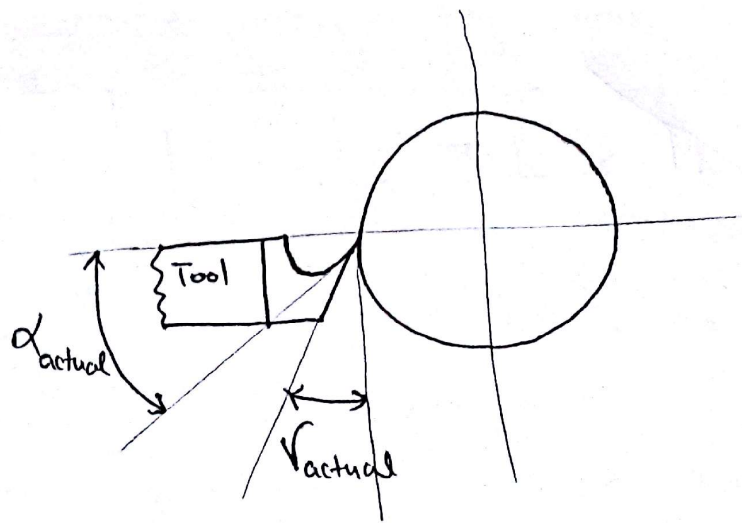
machining time

$$= \frac{L_c}{V} = \frac{t + l_f + l_s + l_r}{V}$$

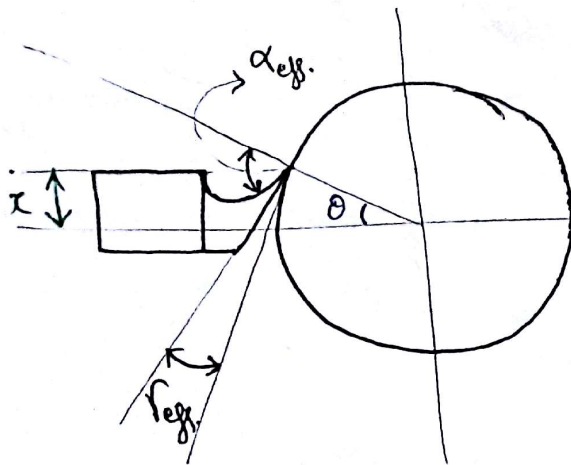
- multipoint cutting tool
- cut slots, grooves, gears, can m/c circular & non circular holes
- $n_r > n_s > n_f$

• Tool offset errors

ideal condition



1) Tool offset above

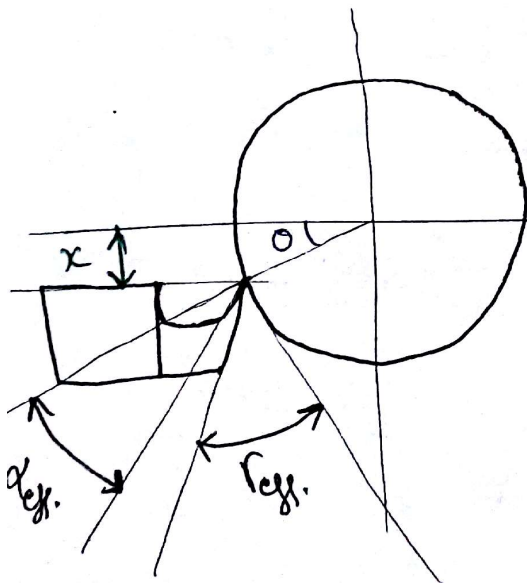


$$\alpha_{eff} = \alpha_{actual} + \theta$$

$$r_{eff.} = r_{actual} - \theta$$

$$\theta = \sin^{-1}\left(\frac{x}{R}\right)$$

2) Tool offset below



$$\alpha_{eff} = \alpha_{actual} - \theta$$

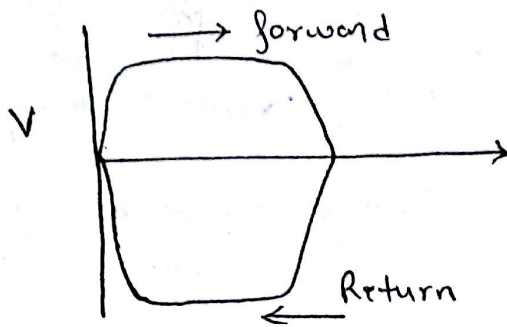
$$r_{eff.} = r_{actual} + \theta$$

$$\theta = \sin^{-1}\left(\frac{x}{R}\right)$$

Shaping

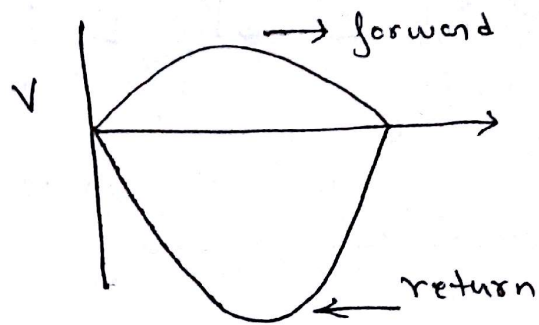
- feed is given to table by "Ratchet & Pawl" mechanism
- Reciprocation to tool is given by "Whitworth O.R.M.M."
- Clapper box is used to lift tool during return stroke
- used to m/c small flat w/p.

Hydraulic shaper



- withstand heavy loads
- involves constant speed throughout
- more no. of strokes can be obtained at given speed of cutting
- can withstand the vibrations induced due to intermittent motion

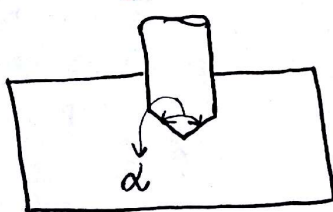
mechanical shaper



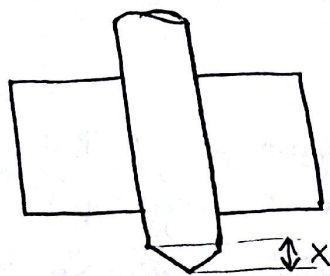
- Speed is max. at midstage of stroke
- simple in construction

- Planner : → w/p reciprocates
→ tool is given feed motion
→ heavier and more rigid than shaper
→ Very large compared to shaper
- Slotter : → invented before shaper
→ Ram reciprocates vertically
→ NO ORMM used

Drilling



blind hole



Through hole

$$\text{machining time} = t_m$$

$$t_m = \frac{L_c}{f N}$$

$\downarrow$ $\frac{\text{mm}}{\text{rev}}$ $\downarrow$ rpm

$$L_c = L_a + L_o + X + t$$

approach

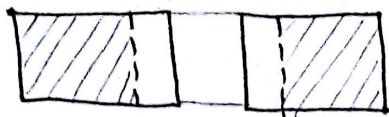
overtraves

$$\text{compulsory approach} = \frac{0.5 D}{\tan \frac{\alpha}{2}}$$

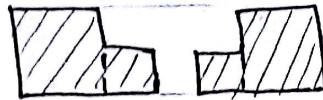
- if point angle / lip angle not given

$$X = 0.3 D \quad \text{for blind hole}$$

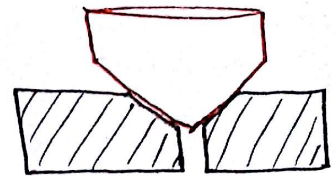
$$X = 0.5 D \quad \text{for through hole} \quad \Rightarrow \text{steels}$$



Boring



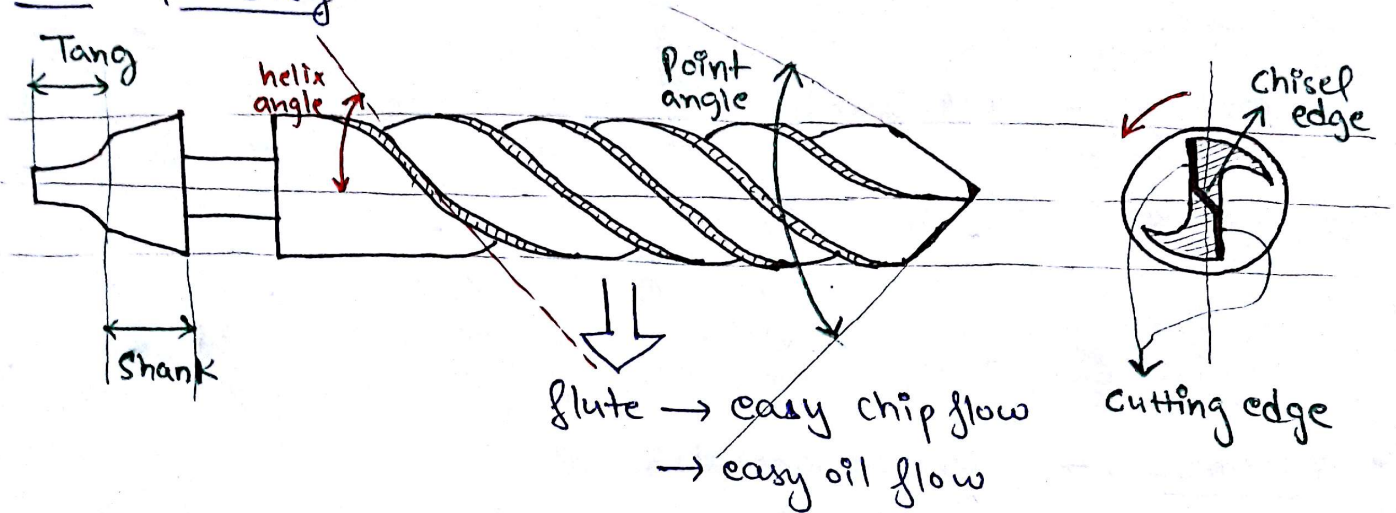
Counter Boring



Counter Sinking

- Spot facing is used to remove burrs from counter boring holes so that nuts can fit easily.

• Drill Geometry



⇒ Rake angle is minimum at dead center and it increases to maximum at periphery and becomes equal to helix angle

⇒ Soft & Ductile w/p ⇒ Point angle ↓
 Rake angle ↑
 helix angle ↑ (b/w 34 to 38°)
 Known as fast helix drill [high twist low strength]
 high lifting of chips

⇒ Hard & strong w/p

⇒ Point angle ↑
 Rake angle ↓
 helix angle ↓ (b/w 12 - 22°)
 Known as slow helix drill
 [low twist strong]
 low lifting of chips

• Deep hole drilling

1) Gun drilling → $3\text{mm} \leq \text{Drill} \leq 50\text{mm}$

2) BTA → $15\text{mm} \leq \text{Drill} \leq 600\text{mm}$

- Trepanning : large diameter holes are produced without drilling, only periphery material is removed.
- Tapping : used for making internal threads
- Lapping : Sizing & finishing a hole already hardened

Reaming

→ it is an operation performed for sizing & finishing the hole, improves dimensional tolerance and accuracy.

Reamers

Right Hand

- blind holes
- pull chips toward shank

Left hand

- milling through holes
- push chips out of hole at other end

Straight

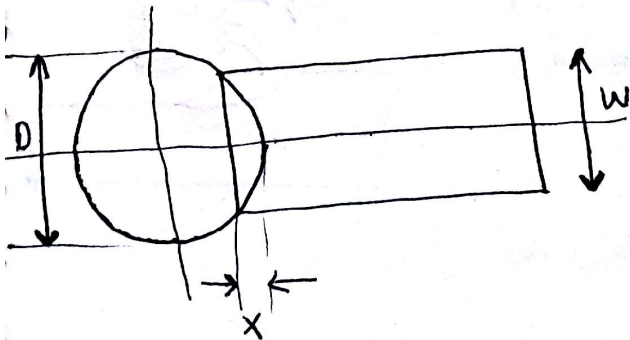
- rake angle is zero
- flutes are parallel to axis

- Reamers are having even number of flutes to reduce the cutting forces.

Milling

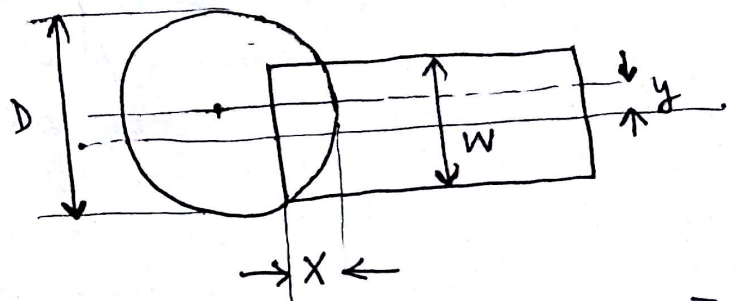
1. Face milling [vertical milling]

Symmetric



$$X = \frac{1}{2} [D - \sqrt{D^2 - W^2}]$$

Asymmetric



$$X = \frac{1}{2} [D - \sqrt{D^2 - (W + 2y)^2}]$$

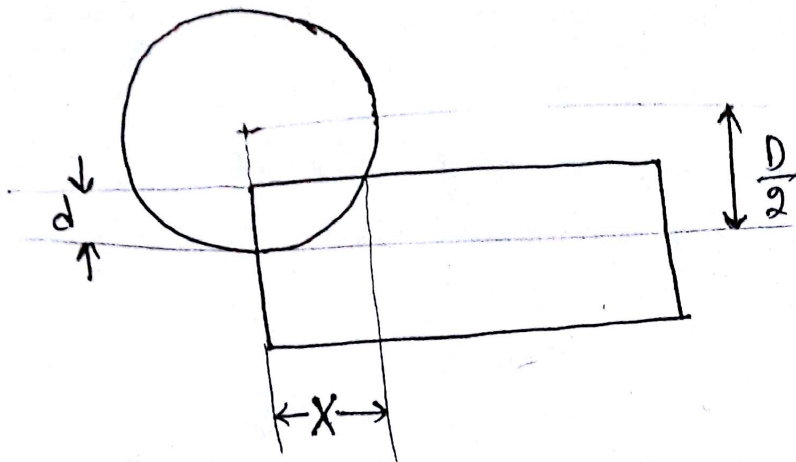
$$t_m = \frac{l_c}{f_m} = \frac{l_c}{f_t \cdot Z \cdot N} = \frac{l + l_o + l_a + X}{f_m}$$

$\downarrow$ mm/min $\downarrow$ rpm $\downarrow$ no. of tooth

$$[\therefore f_m = f_t \cdot Z \cdot N]$$

• When $D < W$ then $X = \frac{D}{2}$

2. Peripheral milling [Horizontal milling]



$$X = \sqrt{Dd - d^2}$$

$$t_m = \frac{l + l_a + l_o + X}{f_m}$$

$$f_m = f_t \cdot Z \cdot N$$

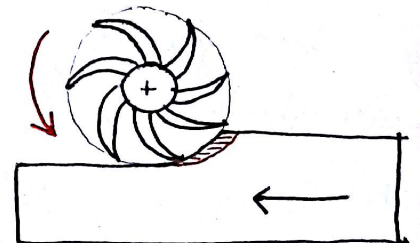
here, maximum chip thickness = $\frac{2f_m}{N_z} \sqrt{\frac{d}{D}}$

minimum chip thickness = 0

avg chip thickness = $\frac{\text{max} + \text{min}}{2} = \frac{f_m}{N_z} \sqrt{\frac{d}{D}}$

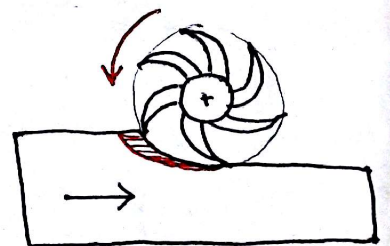
⇒ Upmilling - chip thickness varies from minimum to maximum

- Tool life is less
- surface finish is poor
- cutter tends to lift w/p



⇒ Downmilling - Dirⁿ of cutter & w/p are same

- chip thickness is max at start & mini at end
- higher tool life
- better surface finish
- cutter tends to push w/p towards table



Indexing

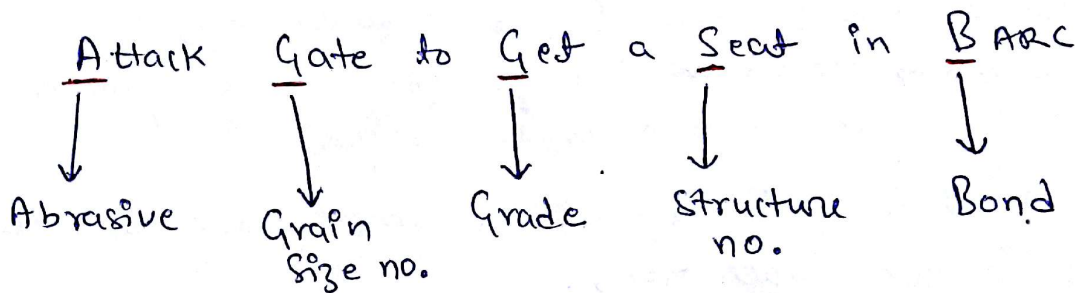
1. Direct indexing : Bevel gears are used
Speed ratio ⇒ 24:1

2. Simple / plain indexing: worm & worm wheel are used
Speed ratio ⇒ 40:1

Grinding

- Highest cutting speed
- highest specific cutting energy ($\frac{J}{mm^3}$)
- Grinding ratio = $\frac{\text{Vol. of material removed from w/p}}{\text{Vol. of grinding wheel wear}}$
- Reason for low MRR
 - Size effect
 - welding effect
 - Negative rake angle

Grinding wheel specification



1. Abrasive
 - Very hard w/p
 - Hard w/p
 - Soft & medium w/p
 - HSS, Bronze, Brass, MS, CI

CBN / Carbide
 Al₂O₃
 Diamond

SiC
 B₄C

2. Grain Size

$$\text{Grain Size} = \frac{1}{\text{GSN}} \text{ inches}$$

$$1 \text{ inch} = 25.4 \text{ mm}$$

3. Grade / Handiers

A to H → soft wheel [for hard w/p]

I to P → medium wheel

Q to Z → Hard wheel [for soft w/p]

- Rubbing, glazing, blunting ⇒ when H-H combination used
- Dressing → removing of worn out abrasive from wheel by single point cutting tool

4. Structure number

0-7 ⇒ Dense structure

8-16 ⇒ Open structure

- Dense structure $\Rightarrow$ for finish grinding & Hard w/p
- Open structure $\Rightarrow$ for rough grinding & soft w/p
- Avg gap b/w abrasive = $\frac{\text{Structure no.}}{1000}$ inches
- Reason for loading
 - $\rightarrow$ mismatch of structure
 - $\rightarrow$ low rpm of wheel
 - $\rightarrow$ improper cutting fluid supply.

5. Bond

Vitrified bond $\rightarrow$ hard & Brittle [but cannot be used at high speed]

Rubber bond $\rightarrow$ soft wheel [used for polishing]

Silicate bond $\rightarrow$ medium & high speed grinding wheel, it is known as water glass.

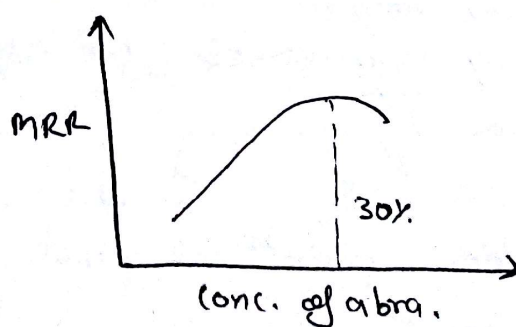
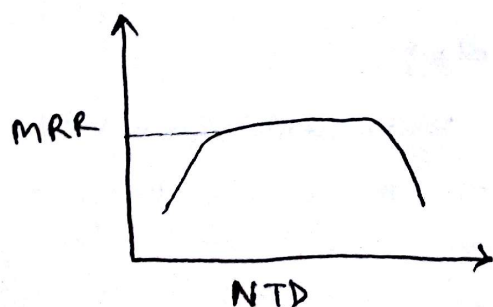
- Grinding wheel life is defined as time period b/w two successive dressing operations.

Centerless grinding

- Direction of w/p is opposite to all other wheels (guiding or regulating wheel & grinding wheel)
- Solid cylinder $\Rightarrow$ External C.G. $\Rightarrow R_w < C_w$
- hollow cylinder $\Rightarrow$ internal C.G. $\Rightarrow R_w > C_w$

Non-Traditional m/cing Process

1. Abrasive jet machining (AJM)



- abrasive speed = 100 to 300 m/s
Pressure = 2 to 10 bar [Al_2O_3 , SiC, glass powder]
- hard / Brittle material m/cing which are heat sensitive
ex:- glass, quartz, cleaning & polishing plastics, deburring

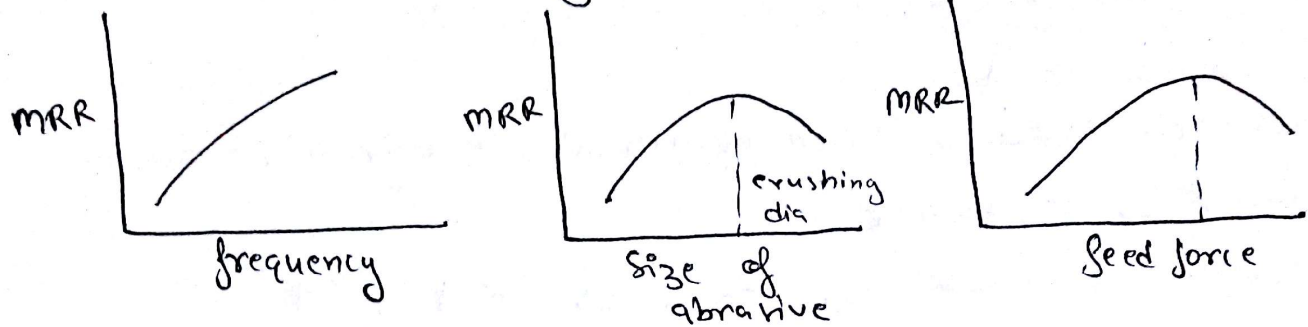
2. Abrasive water JET m/cing

- cutting thick plate of steel, Al, metal matrix composites, fibre plastics.

3. Water jet m/cing

- Cutting thin plates, foils of soft material, paint removal, cleaning, cutting frozen meat, leather.

4. Ultrasonic machining (USM)



- Vibratory frequency $> 16 \text{ KHz}$
- tool vib. $\Rightarrow 20-30 \text{ KHz}$
- tool amplitude $\Rightarrow 0.01 \text{ to } 0.06 \text{ mm}$
- tool is of low carbon or other ductile material
- m/cing of brittle material that has poor electric conductivity and cannot be machined by ECM/EDM.

5. Electro-chemical machining (ECM)

- High current, low voltage process
- MRR sequence $\Rightarrow \text{PAM} > \text{ECM} > \text{EDM} > \text{USM} > \text{EBM} > \text{LBM}$
- material removal by dissolution anode (w/p) in electrolyte
- MRR is independent of w/p physical properties
- Practically no tool wear [Cu, brass, steel]

$$\bullet \quad \text{MRR} = SQ = \frac{AI}{FZ} \quad ; \quad \begin{array}{l} S = \text{gm/cm}^3 \\ Q = \text{cm}^3/\text{s} \\ A = \text{Atomic wt.} \end{array} \quad \left| \begin{array}{l} I = \text{current} \\ F = 96500 \\ Z = \text{valency} \end{array} \right.$$

$$\bullet \quad I = I \times A$$

$$\bullet \quad I = \frac{K(V \pm \Delta V)}{y} \quad \text{here, } \frac{1}{K} = \text{Specific resistance } (\Omega\text{-cm}) \text{ of electrolyte}$$

$y = \text{inter electrode gap (cm)}$

$\Delta V = \text{over voltage } (-\Delta V) \Rightarrow \text{under voltage } (+\Delta V)$

$$\bullet \quad \left(\frac{Z}{A} \right)_{\text{alloy}} = x\% \left(\frac{Z}{A} \right)_p + (100-x)\% \left(\frac{Z}{A} \right)_q$$

- Application - machining conducting material
 - complex profile like, turbine blade, nozzle, complex cavities, high strength material
 - drilling holes
 - die sinking

6. Electric Discharge machining (EDM)

- high voltage, low current process
- w/p $\Rightarrow$ anode
- dielectric used $\Rightarrow$ Transformer oil, Paraffin oil, Kerosine
- temp $\Rightarrow 10,000^\circ\text{C}$
- for High MRR $\Rightarrow$ tool $\Rightarrow K \uparrow, C \uparrow$
w/p $\Rightarrow K \downarrow, C \downarrow$
- Application $\rightarrow$ stamping tools,
 - forging dies
 - mould cavities
 - slots of every type

$\rightarrow \text{MRR} = \frac{40I}{T_m^{1.23}} \text{ cm}^3/\text{min}$ here $T_m = \text{melting point of w/p in } ^\circ\text{C}$

$\rightarrow$ total time = idle time + discharge time

$\rightarrow$ Idle time or cycle time = $RC \ln\left(\frac{V_s}{V_s - V_c}\right)$ Sec.

$R =$ charging resistance

$C =$ charging capacitance

$V_s =$ Supply voltage / open circuit voltage

$V_c =$ charging voltage

$\rightarrow$ Avg power input = $\frac{\text{Total energy consumed per cycle}}{\text{Cycle time}}$

$\rightarrow$ total energy consumed = $\frac{1}{2} C V_c^2$ (J/cycle)

$\rightarrow$ on time or discharge time = $R_m C \ln\left(\frac{V_c}{V_d}\right)$

$R_m =$ m/c resistance

$V_d =$ discharge voltage

$\rightarrow$ to get maximum power $\Rightarrow V_c = 0.716 V_s$

• for wire EDM $\Rightarrow MRR = (X - s/c \text{ of cut}) \times (\text{wire feed})$

$X - s/c \text{ of cut} = \text{width of cut} \times \text{w/p thickness}$

$\text{width of cut} = \text{wire dia} + 2(\text{spark gap})$

7. Electron Beam machining (EBM)

- Electron gun (tungsten or tantalum filament)
- $2^\circ - 4^\circ$ taper for sheet thickness $> 0.1 \text{ mm}$
- fine gas orifice $< 0.002 \text{ mm}$ in space nuclear reactor
- holes in injector nozzle in diesel engines
- turbine blades
- narrow slots

8. Laser Beam machining (LBM)

- focus $\Rightarrow \frac{1}{100} \text{ mm}^2$ size
- Taper $\Rightarrow 1^\circ - 2^\circ$ when thickness exceeds 0.25 mm
- Extremely small holes in hard materials
- fuel filters
- Carburetors
- jet engine blade cooling holes

9. Plasma Arc welding (PAW)

- temp $\Rightarrow 11000^\circ\text{C}$ to 30000°C
- Practically used upto 16000°C
- Profile cutting of stainless steel, Al Alloy, tantalum etc.

Screw thread manufacturing

- External thread cutting process
 - 1) Thread churning [High Quality]
 - 2) Thread rolling
 - 3) Thread grinding
 - 4) open die threading
- Internal thread cutting process
 - 1) Tapping
- Both internal & external
 - 1) Thread milling

Gear manufacturing Process

- External Gear Processes
 - 1) Gear Planning
 - 2) Gear hobbing [highly accurate due to indexing mechanism]
 - 3) Gear milling
 - 4) Gear broaching
- Both internal & external
 - 1) Gear shaping