

Some important point

Lecture 7

22/04/19

① Capacity of lane = Green Ratio $\times$ Saturation flow Rate

$$C = \left(\frac{G_i}{T} \times \frac{3600}{h_i} \right)$$

② Cycle time on the basis of startup lost time

$$T = \left(\frac{n t_{se}}{1 - \sum \frac{V_{ci}}{S_i}} \right)$$

G_i = effective green time, T = cycle time, H_i = saturation time headway

C = traffic capacity of lane in (vehicle/hr)

n = No. of Phase

t_{se} = startup lost time

V_{ci} = critical lane volm

S_i = saturation flow rate

$$\left(S_i = \frac{3600}{h_i} \right)$$

(47)

$$T = 60 \text{ sec}$$

$$G_i = G + A - (t_{s1} + t_{s2}) = 27 + 9 - (2 + 1) = 28 \text{ sec}$$

$$h_i = 2.4 \text{ sec}$$

$$C = \left(\frac{G_i}{T} \times \frac{3600}{h_i} \right) = \frac{28}{60} \times \frac{3600}{2.4} = 700 \text{ veh/hr}$$

(48)



P-1



P-2

$$V_1 = 575$$

$$V_2 = 650$$

$$\sum \frac{V_{ci}}{S_i} = \frac{575}{\left(\frac{3600}{2.3} \right)} + \frac{650}{\left(\frac{3600}{2.3} \right)}$$

$$T = \left(\frac{n t_{se}}{1 - \sum \frac{V_{ci}}{S_i}} \right) = \frac{2 \times 3}{1 - \left(\frac{575 + 650}{\left(\frac{3600}{2.3} \right)} \right)}$$

$$= 27.6 \text{ sec}$$

Design of signal timing by

Webster method $\rightarrow$ this method is based on total lost time

As per this method

optimum cycle time

$$C_o = \left(\frac{1.5L + 5}{1 - Y} \right) \text{ sec}$$

when L = total lost time (including all phases)

$$L = (2n + 1) \times \text{All per time}$$

No. of phase

Y = sum of critical flow ratio

$$Y = Y_1 + Y_2 = \text{for 2 phase}$$

$$y_1 + y_2 + y_3 + y_4 = 4 \text{ phases}$$

y_c critical flow ratio = $\left(\frac{\text{normal traffic flow}}{\text{saturated flow rate}} \right)$

Green time

$$\left. \begin{aligned} g_1 &= \frac{y_1}{Y} (C - L) \\ g_2 &= \frac{y_2}{Y} (C - L) \end{aligned} \right\} \begin{aligned} &\text{as per the max} \\ &\text{min amber time} \\ &= 2 \text{ sec per phase} \end{aligned}$$

Pb (50)

$$L = (2m + R) = 2 \times 2 + 12 = 16 \text{ sec}$$

$$Y = y_1 + y_2$$

$$= \frac{4000}{1250} + \frac{250}{1000} = 0.32 + 0.25 = 0.57$$

optimum cycle time

$$C_0 = \left(\frac{1.5L + 5}{1 - Y} \right) = \left(\frac{1.5 \times (16) + 5}{1 - 0.57} \right) = 67.4 \text{ sec}$$

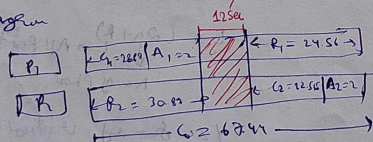
Green time $g_1 = \frac{y_1}{Y} (C_0 - L) = \frac{0.32}{0.57} \times (67.4 - 16) = 28.80 \text{ sec}$

$$g_2 = \frac{y_2}{Y} (C_0 - L) = \frac{0.25}{0.57} \times (67.4 - 16) = 22.56 \text{ sec}$$

Amber time

= 2 sec (min)

phase diagram



Pb - (51)

$$\left(\frac{R}{n} \right) = 3 \text{ sec}$$

$$R = 3n = 3 \times 2 = 6 \text{ sec}$$

$$L = 2m + R = 2(2) + 6 = 10 \text{ sec}$$

$$y_{N-S} = \left\{ \begin{aligned} y_N &= \frac{1000}{3600} = \frac{1}{3} \\ y_S &= \frac{600}{2400} = \frac{1}{4} \end{aligned} \right\} \text{ max} = \frac{1}{3}$$

$$y_{S-N} = \left\{ \begin{aligned} y_E &= \frac{950}{3600} = 0.26 \\ y_W &= \frac{800}{2000} = \frac{2}{5} \end{aligned} \right\} \text{ max} = \left(\frac{2}{5} \right)$$

Optimum cycle time

$$C_0 = \frac{1.5L + 5}{1 - Y} = \frac{1.5(10) + 5}{1 - \left(\frac{1}{3} + \frac{2}{5} \right)} = 75 \text{ sec}$$

TRAFFIC SIGN

① Mandatory sign

Regulatory sign shape circular



① Exceptional

① Stop sign



- Red background
- White boundary
- Octagonal

② Give Way sign



- Red boundary
- White background
- Inverted triangle

③ Warning sign

shape - triangular



- Red boundary
- White background

③ Glosomatically sign



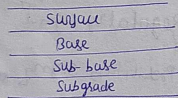
Pavement Design

- ① Flexible Pavement
- ② Rigid Pavement
- ③ Semi-Rigid Pavement
- ④ Composite Pavement

Flexible

- ① Flexible rigidity
- ② Load transfer - estimation
- ③ No. of layers

very low or negligible
Through again to gain contact



Failure

As there is any failure at bottom then the failure will appear at the top

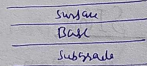
Joint

Cost

- ① No joint requires low initial cost high maintenance cost

Rigid

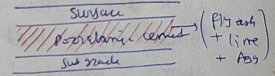
Significant
layer to layer



As there is any failure at bottom then concrete slab will act as a bridge over small cavity

- ① expansion and contraction joint are provided
- ① High initial cost low maintenance cost

- ③ Semirigid Pavement If subbase course and base course of flexible pavement is replaced by Pozzolanic concrete (Fly ash + lime + egg) then strength of pavement increases this strength is more than flexible pavement but less than rigid pavement.



- ④ Composite Pavement If bituminous concrete is provided at top layer over cement concrete slab then it is called composite pavement

design of flexible Pavement:

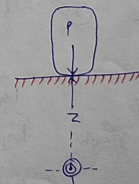
- ① Design Parameter :- ① max std. axle load

$$= 8170 \text{ Kg}$$

$$= 8.2 \text{ T}$$

$$= 80 \text{ Km}$$

- ② Stress at any depth



$$\sigma_z = p \left(1 - \frac{z^3}{(r^2 + z^2)^{3/2}} \right)$$

$$p = \text{contact pressure} = \frac{P}{A}$$

$$P = \text{wheel load}$$

$$A = \text{contact area} = \pi r^2$$

$$r = \text{radius of contact area}$$

$$z = \text{depth}$$

- ③ Rigidity Factor (R.F)

$$R.F = \left(\frac{\text{contact pressure}}{\text{tyre pressure}} \right)$$

$$\text{for design: } C.P = T.P = 7 \text{ Kg/cm}^2$$

R.F	C.P	T.P
1	7	7
> 1	> 7	< 7
< 1	< 7	> 7

- ④ Mc load theorem

$$L \propto \frac{1}{N}$$

$$L_1 M_1 \geq L_2 M_2$$

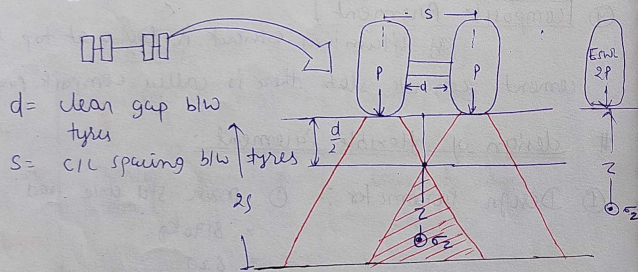
$$\left(L = \text{axle load} \right)$$

$$\left(N = \text{No. of repetition} \right)$$

ESWL (Equivalent single wheel load)

Load on single tyre which

will cause an equivalent magnitude of parameter such as stress-strain and deflection at the given location to that resulting from multiple wheel load of same wheel load.

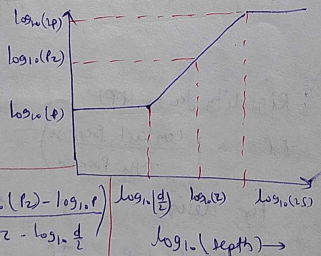


Observation

① upto depth $\frac{d}{2}$
ESWL = P

② Beyond depth z_s
ESWL = 2P

③ $\frac{d}{2} < z < z_s$
ESWL from graph



$$\frac{\log_{10} 2P - \log_{10} P}{\log_{10}(2S) - \log_{10}(\frac{d}{2})} = \frac{\log_{10}(P_2) - \log_{10} P}{\log_{10} z - \log_{10} \frac{d}{2}}$$

Pb - (30)

P = 2004 Kg

S = 27 cm

d = 11 cm

z1 = 5 cm

z2 = 30 cm

zs = 60 cm

① At $z = 5 \text{ cm} < \frac{d}{2}$

$$ESWL = P = 2004 \text{ Kg}$$

②

At $z = 60 \text{ cm} > z_s$

$$ESWL = 2P = 2 \times 2004 = 4008 \text{ Kg}$$

③

$\frac{d}{2} < z = 30 \text{ cm} < z_s$

$$\frac{\log_{10}(2 \times 2004) - \log_{10}(2004)}{\log_{10}(2 \times 27) - \log_{10}(\frac{11}{2})} = \frac{\log_{10}(P_2) - \log_{10}(2004)}{\log_{10} 30 - \log_{10}(\frac{11}{2})}$$

$$\log_{10} P_2 = 3.527$$

$$P_2 = 3353.24 \text{ Kg}$$

Remember -
 $\log_{10} \frac{a}{b} = \log_{10} a - \log_{10} b$
change $\frac{a}{b}$ to $\log_{10} a - \log_{10} b$

Design of Pavement thickness:

Method ① Group index method - this method is based on index property of soil.

① index property are those which are used only for classification of soil such as liquid limit, plastic limit, plasticity index etc

$$GI \text{ value} = 0.2a + 0.005ac + 0.01bd$$

$$a = (P - 35) \times 40$$

$$b = (P - 15) \times 40$$

$$c = [W_L - 40] \times 20$$

$$d = (I_p - 10) \times 20$$

P = % fines passing 75 μ sieve

W_L = liquid limit

I_p = Plasticity index

I_p = (W_L - W_p)

Note: ① GI value lies b/w (0-20)

② higher the GI value poorer the soil hence higher thickness of pavement required

③ total thickness of pavement depend up on GI value only. St thickness of surface course and base course depend upon GI value and traffic volume both.

Limitation: quality of pavement is not considered
same thickness require if even if better
quality of material used.