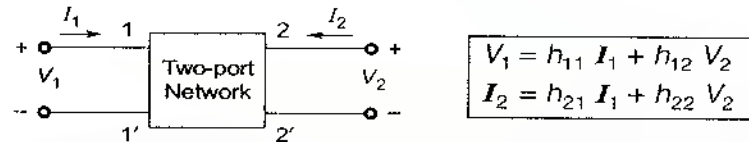


# Transistor Hybrid Model

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## Introduction

The  $h$ -parameter model of BJT is defined by two-port network as



Input impedance  $h_{11}/h_i$

$$h_{11} = \left. \frac{V_1}{I_1} \right|_{V_2=0}$$

Current gain  $h_{21}/h_f$

$$h_{21} = \left. \frac{I_2}{I_1} \right|_{V_2=0}$$

Reverse voltage gain  $h_{12}/h_r$

$$h_{12} = \left. \frac{V_1}{V_2} \right|_{I_1=0}$$

Output Admittance  $h_{22}/h_o$

$$h_{22} = \left. \frac{I_2}{V_2} \right|_{I_1=0}$$

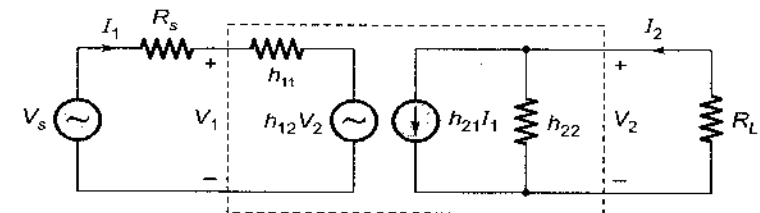
## Typical h-parameter Values for Transistors

| Parameters     | CE                   | CC             | CB                   |
|----------------|----------------------|----------------|----------------------|
| $h_{11} = h_i$ | 1.1 k $\Omega$       | 1.1 k $\Omega$ | 21.6 $\Omega$        |
| $h_{12} = h_r$ | $2.5 \times 10^{-4}$ | 1              | $2.9 \times 10^{-4}$ |
| $h_{21} = h_f$ | 50                   | -51            | -0.98                |
| $h_{22} = h_o$ | 24 $\mu$ A/V         | 24 $\mu$ A/V   | 0.49 $\mu$ A/V       |
| $1/h_o$        | 40 k $\Omega$        | 40 k $\Omega$  | 2.04 M $\Omega$      |

## Approximated Conversion Formulaes for h-paramters

| CE to CC                 | CE to CB                                             |
|--------------------------|------------------------------------------------------|
| $h_{ic} = h_{ie}$        | $h_{ib} = \frac{h_{ie}}{1 + h_{fe}}$                 |
| $h_{rc} = 1$             | $h_{rb} = \frac{h_{ie} h_{oe}}{1 + h_{fe}} - h_{re}$ |
| $h_{fc} = -(1 + h_{fe})$ | $h_{fb} = \frac{-h_{fe}}{1 + h_{fe}}$                |
| $h_{oc} = h_{oe}$        | $h_{ob} = \frac{h_{oe}}{1 + h_{fe}}$                 |

## Hybrid Model



Current gain

$$A_f = \frac{I_2}{I_1} = \frac{-h_{21}}{1 + h_{22} R_L} = \frac{-h_f}{1 + h_o R_L}$$

where,  $I_1$  = AC input current  
 $I_2$  = AC output current

Voltage gain

$$A_v = \frac{V_2}{V_1}$$

where,  $V_1$  = AC input voltage  
 $V_2$  = AC output voltage

$$A_v = \frac{-h_{21} R_L}{h_{11} + (h_{11} h_{22} - h_{12} h_{21}) R_L} = \frac{-h_f R_L}{h_i + (h_i h_o - h_r h_f) R_L}$$

Input impedance

$$Z_{in} = \frac{V_1}{I_1} = h_{11} - \frac{h_{12} h_{21} R_L}{1 + h_{22} R_L} = h_i - \frac{h_r h_f R_L}{1 + h_o R_L}$$

## Output impedance

$$Z_{out} = \frac{V_2}{I_2} = \frac{R_s + h_{11}}{(R_s + h_{11})h_{22} - h_{12}h_{21}} = \frac{R_s + h_i}{(R_s + h_i)h_o - h_r h_f}$$

$$Y_{out} = h_o - \frac{h_r h_f}{h_i + R_s}$$

## Multistage Amplifier

- Upper cutoff frequency of overall configuration is

$$f_H^* = f_H \sqrt{2^{1/n} - 1} \quad (\text{For identical amplifiers in cascade})$$

where,  $n$  = number of amplifiers in cascade

$f_H$  = upper cutoff frequency of one amplifier

- Lower cutoff frequency of overall configuration

$$f_L^* = \frac{f_L}{\sqrt{2^{1/n} - 1}}$$

where,  $n$  = number of identical amplifiers in cascade

Approximate BW of amplifier in cascade is  $f_H^*$ .

- When amplifiers are non-identical then

$$f_L^* = 1.1 \sqrt{f_{L1}^2 + f_{L2}^2 + f_{L3}^2 + \dots + f_{Ln}^2} \quad \text{and} \quad \frac{1}{f_H^*} = 1.1 \sqrt{\frac{1}{f_{H1}^2} + \frac{1}{f_{H2}^2} + \dots + \frac{1}{f_{Hn}^2}}$$

- Rise time  $t_r^* = 1.1 \sqrt{t_{r1}^2 + t_{r2}^2 + \dots + t_{rn}^2}$

