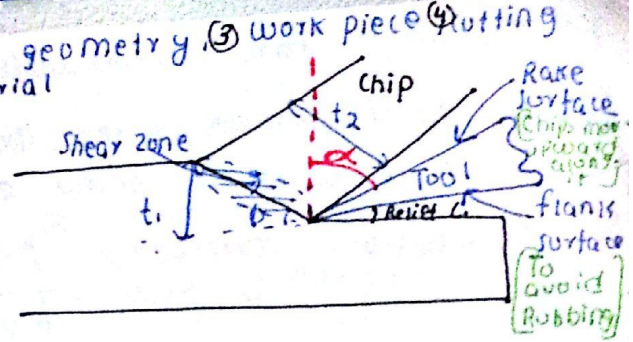
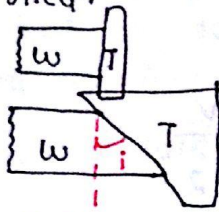


Metal Cutting: ① m/c used, ② cutting tool material and geometry, ③ work piece, ④ cutting parameters, ⑤ work holders, ⑥ Process: Removing material as chips

Mechanics of m/c: Deformation by shear

Classification of m/c:
 Orthogonal
 Oblique



Orthogonal: ① Cutting edge of tool at 90° to tool feed ② chip flow \perp to cutting edge ③ $i = 0$ ④ chips get coiled ⑤ \uparrow Tool life ⑥ 2 force component ⑦ slotting parallel ⑧ at an acute \angle ⑨ $i \neq 0$ ⑩ chip flow side way ⑪ \downarrow heat production ⑫ 3 cutting forces

Forces in single pt. Tool:

F_r = Radial force (Along axis of tool)
 F_f = feed force
 F_c = In direction of depth

F_t = Res. of F_r, F_f

$R = \sqrt{F_r^2 + F_f^2}$

Orthogonal $F_r = 0$ $F_t = F_f$ $R = \sqrt{F_f^2 + F_c^2}$

Cutting force F_c = in direction of cutting velocity, largest, vertical plane, tangential to work surface, Tangential force, 99% of power

Feed force F_f = Hori. plane, \parallel to axis of work, direction of tool feed, 30-60% of F_c

F_r = \perp to m/c surface in hori. plane along Tool axis, 20-40% of F_c .
 $F_r = 0$ for orthogonal

Tool signature: ASA - American standard asso. system ① Tool in hand: Tool is considered idle against w.p. ② based on m/c Ref. plane

ORS - orthogonal Rake system ① Tool is active and works against w.p. ② based on Tool R.P.

ASA

ORS

3 Ref. planes

3 Ref. planes

1-Hori. base plane

1-hori base plane

2-Long. plane

2-cutting plane

(i) \perp to B.P.

(i) \perp to B.P.

(ii) \parallel to feed direction

(ii) passes thru side cutting edge

3-Transverse plane

3-orthogonal plane

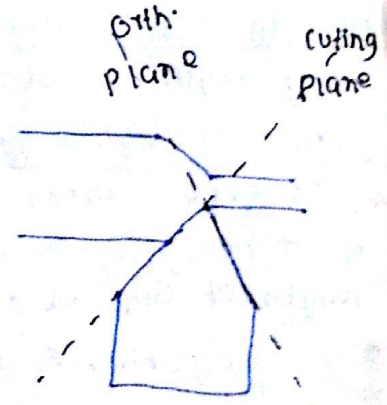
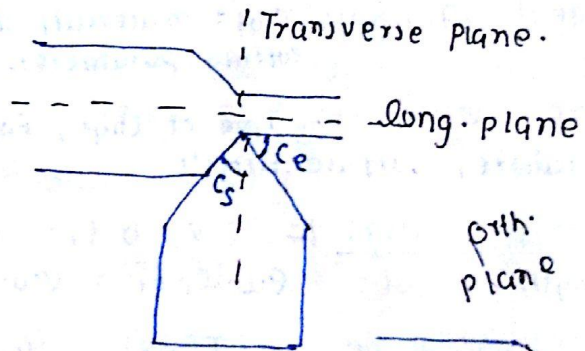
(i) \perp to both planes

(i) \perp to both planes

(ii) \parallel to Transverse motion of tool

ASA - $\alpha_b, \alpha_s, \theta_e, \theta_s, \phi_e, \phi_s, R$

ORS - $I, \alpha_n, \theta_e, \theta_s, \phi_e, h, R$



I = Inclination \angle

α_n = normal rake

λ = approach $\angle = 90 - \phi_s$

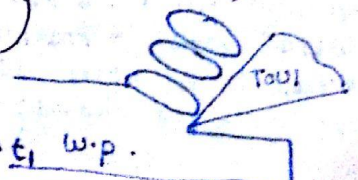
$$\tan I = \cos \phi_s \tan \alpha_b - \sin \phi_s \tan \alpha_s \quad \text{CAB } (\phi_s, \alpha_b) \quad \text{CAS } (\phi_s, \alpha_s)$$

$$\tan \alpha_n = \cos \phi_s \tan \alpha_s + \sin \phi_s \tan \alpha_b \quad \text{(CAS - CAB)}$$

Types of chips: 1- Discontinuous - Brittle fracture, small segments of chips, easy to handle

condn - \downarrow cutting speed, \downarrow Rake \angle , \downarrow feed, Brittle work material, $\uparrow t_1$ w.p.

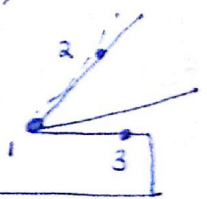
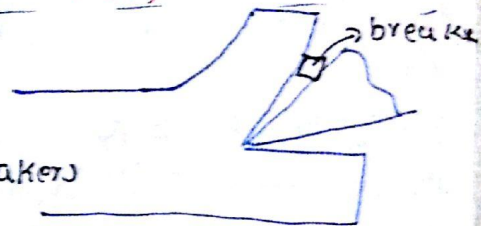
effect - Tool life \downarrow , Power \uparrow , sur-finsh \uparrow



- ① Turbine for underwater power stations → (i) Tubular Turbine.
(ii) Bulb Turbine.
- ② → η of pump is less than that of Turbine generally.
→ More losses in pump due to eddies and Turbulence.
- ③ Cavitation Number = $\frac{p - p_v}{\rho v^2 / 2}$ p = Abs pressure ρ = Density
 p_v = vap. " of fluid v = free stream velocity

④ When a moving Automobile experience wind resistance →
Then use $\frac{F}{\rho v^2 d^2} = \text{const}$. Thus $\frac{F_2}{F_1} = \left(\frac{v_2}{v_1}\right)^2$.

- 2-continuous: ↑ plastic deformation, longer continuous chips, desirable b/c show stable cutting.
spiral coiling can harm operator or finish ∴ chip breakers
- condition - ↑ speed, ↑ Rake \angle , ductile, suitable cutting fluid, ↓ t_c .
- Effects - ↓ power, ↑ Tool life, steady and stable forces, ↓ unblw chip and tool.
- 3- continuous with BUE: Ductile material, ↓ speed, weld spots at tip of tool. ① which later breaks into 4213.
- condition - ↓ speed, ↓ Rake \angle , material with ↑ adhesion
- Effects - ↓ flank wear, ↑ Tool life, ↓ sur-finish, ↑ power & ↑
* disappears with ↑ in speed, rake \angle , suitable cutting fluid.



Independent variables: Tool: material, shape, condⁿ work: material, condⁿ, Temp.
cutting parameters: f , n , c fluid work holding & fixturing

Dependent variables: Type of chip, Force & energy dissipated, Temp. Rise, wear & failure, surface finish

MRR in Tool cutting: # $\rho \cdot v_c \cdot b \cdot t_1 = \rho \cdot v_f \cdot b \cdot t_2 \Rightarrow v_f = v_c \cdot r$
By length of cut: $\rho \cdot b \cdot \ell_1 \cdot t_1 = \rho \cdot b \cdot \ell_2 \cdot t_2 \Rightarrow r = \frac{t_1}{t_2} = \frac{\ell_2}{\ell_1}$

Specific cutting energy: $u_c (J/m^3)$: $u_c = \frac{F_c}{b \cdot t} = \frac{N}{m^2} = \frac{N \cdot m}{m^3} = \frac{J}{m^3}$
 $w = F_c \cdot \ell$ $mrr = u \cdot b \cdot t (m^3/s)$

a- Turning: F_c, F_f given. outer dia D velocity V Rake $\angle \alpha$ depth of cut d
length of chip ℓ_2 . Ans: $F = F_c \sin \alpha + F_f \cos \alpha$ $\lambda = \tan^{-1} \frac{F}{N}$ * $t_1 \cdot b \cdot \pi D = t_2 \cdot b \cdot \ell_2$
 $N = F_c \cos \alpha - F_f \sin \alpha$ $r = \frac{t_1}{t_2} = \frac{\ell_2}{\pi D}$ find d

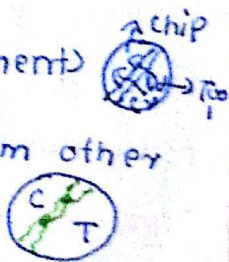
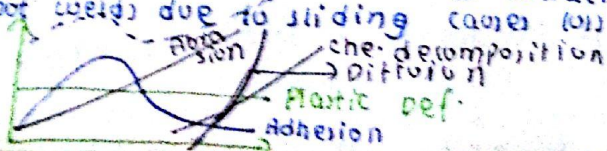
b- Normally: Find F_s using T_s, b, t_1, d . Find F_c by $\frac{F_s}{\cos(\phi + \alpha)} = \frac{F_c}{(\lambda \alpha)}$

Mechanism of Tool wear: 1-Diffusion: -At ↑ T diffusion of Alloying element (from ↑ concn to ↓ concn) towards chip.
-depends on concn gradient & Temp.

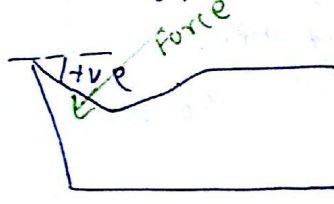
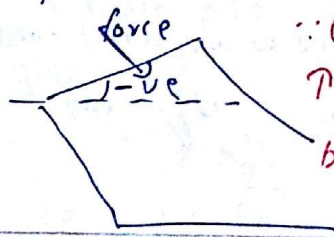
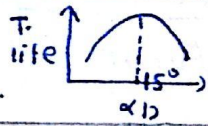
2-Abrasion: If material has very hard particle due to rubbing it dislodges from other

3-Adhesion: -At ↑ TS Pr. metallic bond b/w chip & tool at contact pt).
a) weld spots - Fracture of spot (weld) due to sliding causes loss of material from both surfaces

Wear Rate vs speed:



- ① (i) single pt. Tools : Turning, Boring, Shaping, planing.
(ii) multiple pt. : Drilling, Reaming, Tapping, milling, Broaching, ^{saw}ing.
- ② RAKE L. Guide the chip away from the cutting edge
Thus \downarrow chip pressure on face $\Rightarrow \downarrow$ force, \downarrow power
- Large α : Soft and ductile material, \downarrow power, Easy cutting
Small α : To cut hard material, \uparrow Tool strength, \uparrow Tool life.

- promotes chip formation - Reduces Force, power consumption		+ve Rake	-ve Rake
(i) <u>work material</u>	Soft and ductile	\uparrow strength alloys, hard, brittle	
(ii) <u>Type of cutting</u>	continuous	Interrupted	
(iii) <u>Forces</u>	Shearing, Bending 	compressive (\because For carbide Tool)  \because carbide Promotes but \downarrow Tensile	
(iv) <u>Heat dissipation and Tool life</u>	Poor	Good	
# For \downarrow speed		* For less Tensile strength tools * Best $\alpha_b = 22^\circ$	
# \downarrow F_c , Power needed.			

Note 0° back Rake L \rightarrow Brass, Thread cutting.

- ③ (i) End clearance (ϵ_e) : Allows End of cutting Tool to enter work
(ii) side (ϵ_s) : " side of Tool to advance into "
- ④ (i) side cutting edge L (C_s) : - It determines chip flow direction.
- prevents interference as tool enters w.p.
 $(15^\circ - 30^\circ)$
 \rightarrow Large C_s : \uparrow Tool life, \uparrow chatter, vibration.
 \rightarrow How life \uparrow : By this wider chips produced \rightarrow Heat over large Area
 \rightarrow Imp : Thus no effect on force, power. * $T_{max} \propto \sqrt{f \cdot \cos C_s}$
- (ii) ECER ($80^\circ - 150^\circ$) : Too small affects surface finish.
- ⑤ NOSE RADIUS : \uparrow finish, Tool life, F_c , power, vibration, chattering
Too large \rightarrow chatter
Too small \rightarrow weakens pt.

(i) chip thickness Ratio: $t_1/t_2 = L_2/L_1$

$$\gamma = \frac{t_1}{t_2} = \frac{\sin \phi}{\cos(\phi - \alpha)}$$

$$\tan \phi = \frac{\gamma \cos \alpha}{1 - \gamma \sin \alpha}$$

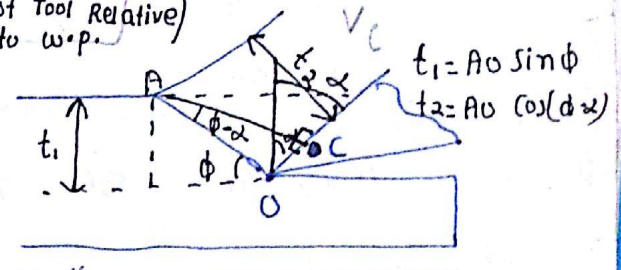
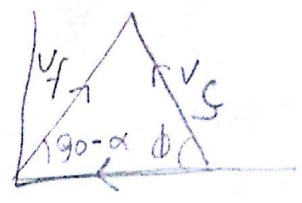
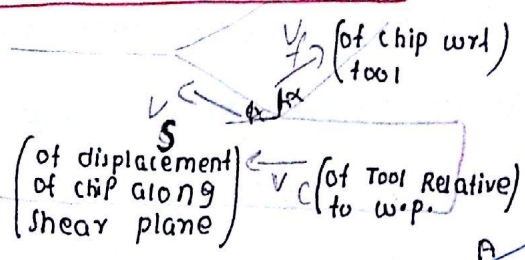
(ii) Shear Strain:

$$\gamma = \tan(\phi - \alpha) + \cot \phi$$

(iii) velocity Relation:

2-D orthogonal cutting:
 - Completely defined by α and ϕ
 - Assume:
 1- perfectly sharp tool
 2- shear zone
 3- no chip side flow

$$V_f = V_c \cdot \gamma$$

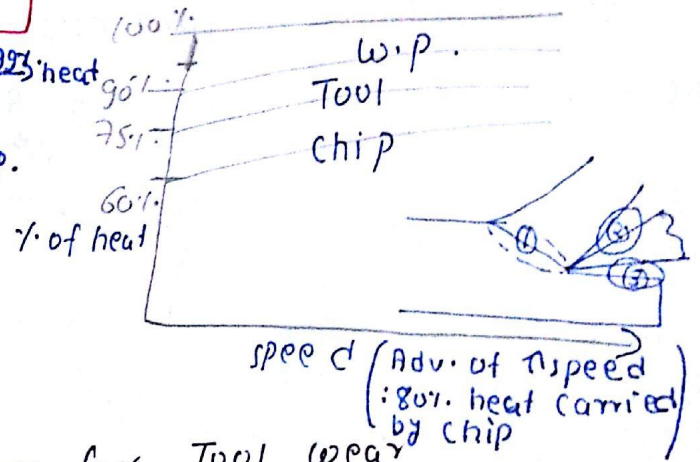


$$t_1 = f \cdot \cos \phi_s$$

$$b = \frac{d}{\cos \phi_s}$$

max. temp. $\propto \sqrt{t_1} \propto \sqrt{f \cdot \cos \phi_s}$
 (7) Heat Generated in milling Power $\frac{925}{100}$ heat

- (i) primary zone (Around shear plane)
 - Partly carried by chip, (Ties) - Rest Retained by w.p.
- (ii) secondary " (Tool chip Interface)
 (Ties with cutting speed)
- (iii) Tertiary " (Tool work)

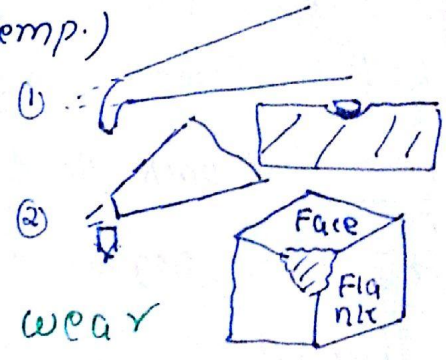


Heat in (ii) > (i) >>> (iii)
 → ↓ Tool life, ↓ Tool hardness

(8) Type of Tool failure (Power \uparrow , Unable to cut, ↓ μ_{fin})

(9) Reason for Tool wear

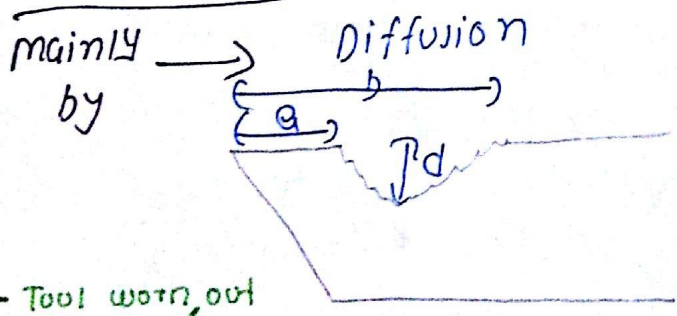
- (i) plastic deformation (Due to $\uparrow T$)
- (ii) mechanical breakage (Due to \uparrow Forces)
- (iii) Gradual wear (c.w., f.w.)
- (i)(ii) can be eliminated but not (iii)
- (i) Diffusion (at \uparrow Temp.)
- (ii) Adhesion
- (iii) Abrasion



(10) TYPE OF WEAR

(i) CRATER WEAR

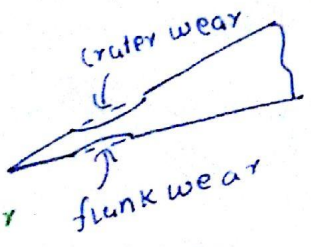
(ii) Flank wear



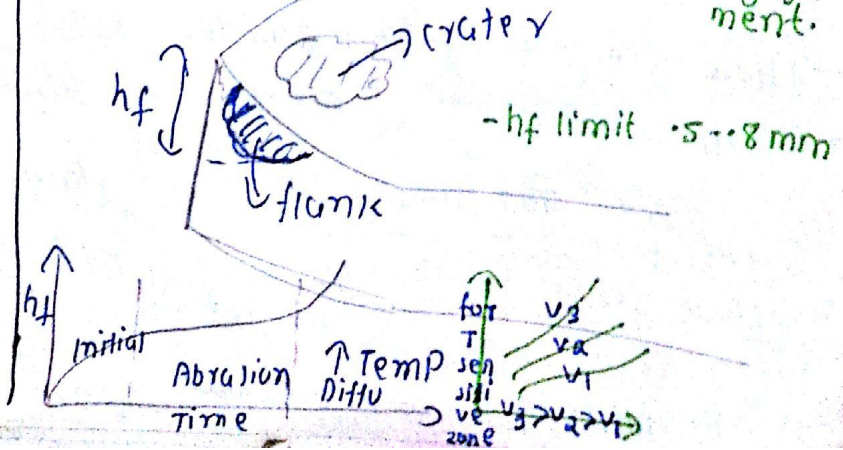
- Tool worn out if $X > .4 - .6$

$$X = \frac{2d}{a+b}$$

 - At tool face at a short distance by chips flowing over face due to $\uparrow T$.



- Abrasion, Adhesion, at $\uparrow T$ diffusion
- At corner and notch of tool
- Due to work hardening & sudden engagement.



① Cutting Tool material **PROPERTIES:** HOT OR RED HARDNESS, WEAR RESISTANCE, Toughness, γ_K , γ_{CP} , γ_M , Thermal stability $3\alpha, 1.352 \frac{H_T}{H_{WP}}$

→ CS, HSS, (cast alloys (Stellite), cemented carbide (P, M, K), (coated carbide, ceramic) (cemented oxide) (Diamond, CBN, UCON. (made by Rolling)

(By P-metallurgy, sintering) (for carbides) (WC, TiC, TaC) (TiC, TiN, TiCN)

→ 1.35 \angle Hardness Tool \angle 1.5 # (i) CS, HSS → Forging

H w.p (ii) Stellite → casting

(iii) ceramic, carbide → powder

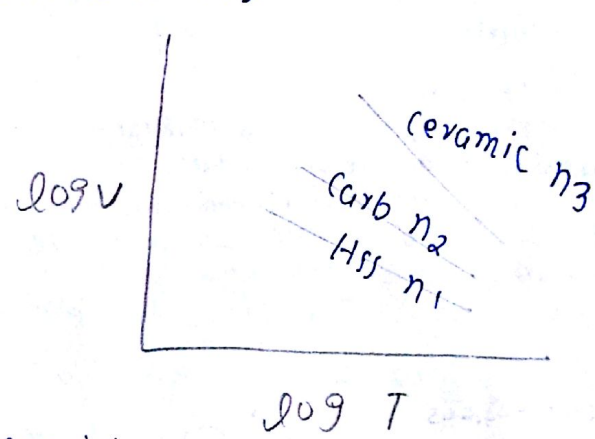
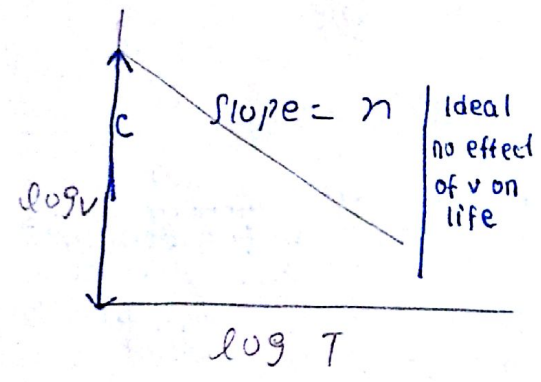
(iv) UCON → Rolling

② Tool life $V \cdot T^n \cdot f^P \cdot d^Q = C$

→ Effect on Tool life: $V > f > d$

→ n: HSS [0.8-1.2], Carbide [1.2-1.5], ceramic [1.5-1.8]

→ superior: ceramic > carbide > HSS



$n_3 > n_2 > n_1$

→ $\downarrow n \Rightarrow$ Tool life sensitive to cutting speed

→ $\uparrow C \Rightarrow$ \uparrow Tool life.

③ Machinability Factors affecting it: (Ease of m/cing a given material)

- | | |
|---------------------|--|
| (i) Tool life | $\left[\begin{aligned} C_m &= \text{M/cing cost per unit time} \\ C_e &= \text{Regrinding cost per grinding} \\ T_m &= \text{M/cing time in mins/unit} \\ T_i &= \text{Idle time in mins/unit [loading + unloading]} \\ T_c &= \text{Tool changing Time in mins/failure} \end{aligned} \right.$ |
| (ii) surface finish | |
| (iii) cutting force | |
| (iv) power needed | |
| (v) MRR | |

→ $T_m = \frac{L}{f \cdot n} = \frac{L \pi D}{f \cdot v}$ → No. of Tool failures per work piece = $\frac{T_m}{T} = \frac{T_m \cdot v^{1/n}}{C^{1/n}}$

→ Total cost = $C_m \cdot T_m + C_m \cdot T_i + C_m \cdot \frac{T_m}{T} \cdot T_c + \frac{T_m}{T} \cdot C_e$

Per unit $T_m + T_i + \frac{T_m}{T} \cdot T_c$

→ Time =

→ Rate of production $R_p = \frac{1}{T}$

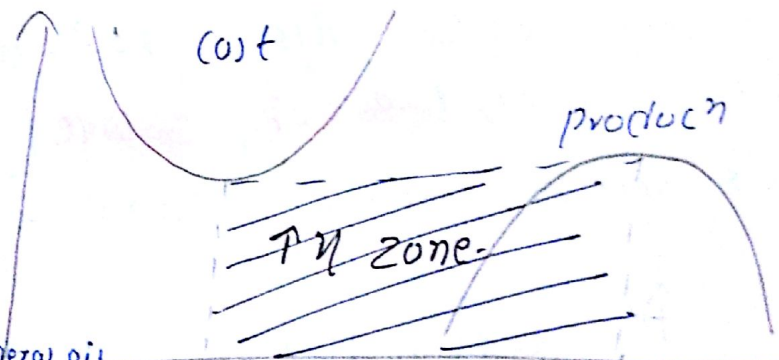
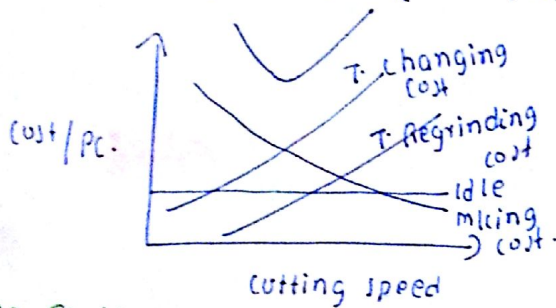
(i) for min. cost $\left[\frac{dC_p}{dv} = 0 \right]$ $\left[\frac{\partial R_p}{\partial v} = 0 \right]$ (ii) for max. production

$$v_{mc} = \frac{C}{\left[\left\{ \frac{1}{n} - 1 \right\} \left\{ T_c + \frac{C_e}{C_m} \right\} \right]^n}$$

$$v_{mp} = \frac{C}{\left[\left(\frac{1}{n} - 1 \right) \cdot T_c \right]^n}$$

$$T_{mc} = \left\{ \frac{1}{n} - 1 \right\} \left\{ T_c + \frac{C_e}{C_m} \right\}$$

$$T_{mp} = \left\{ \frac{1}{n} - 1 \right\} \cdot T_c$$



Cutting Fluids:

- 1- water based \rightarrow Solutions, Emulsions
- 2- mineral oil based \rightarrow inactive oil \rightarrow mineral oil, fatty oil

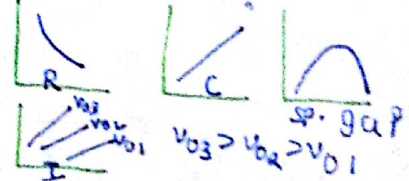
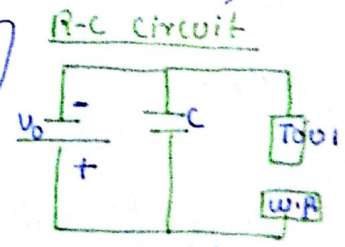
④ USM → Frequency: 20-30 KHZ → Amplitude: 25-100 μ m
(Beyond hearing Range: no noise)
→ Apply: Dentistry, Jewellery, Stone cutting, Die making
Tool: Should stand vib. & corrosion
- coating to avoid wear - SiC, AlN
→ Can't use for: Ductile
- low MRR
→ ↑ surface finish, Easy for hard material
Adv: ↑ accuracy, safe & noiseless, heat gen.

⑤ AJM 2-10 MPa, 150-300 m/s, 30 L/min, 8-13 mm
Abrasive: Al_2O_3 , SiC, $NaHCO_3$, glass beads
Temp. of spark (8000-1500°C), spark gap (0.25-0.5 μ m),
⑥ EDM D.C. supply (30-240 V), MRR (300 mm³/min)

→ Imp: For max. power $V_d = 0.72 V_0$
→ Apply (i) only for electrical conductor
(ii) wire drawing, sinking, extrusion dies
(iii) micro holes for nozzle, narrow slots.
(iv) Hard carbides, Aerospace industry

⑦ MRR PAM > ECM > EDM > [AJM > USM] > EBM > LBM
can interchange

PENE LBM > EBM > USM > ECM > EAM > PAM > AJM
→ (i) AJM goes to last (iii) Reverse MRR for PENE.
(ii) ECM > EDM in both



① (i) $F = F_T \sin \alpha + F_C \cos \alpha$ $F_C \sin \alpha + F_T \cos \alpha$
 (ii) $N = F_T \cos \alpha - F_C \sin \alpha$ $F_C \cos \alpha - F_T \sin \alpha$
 (iii) $F_S = F_S = \frac{F_C \cdot t \cdot b}{\sin \phi} = F_C \cdot \omega$
 (iv) $F_N =$



- ② (i) Ernest and Merchant : $2\phi + \lambda - \alpha = \pi/2$
 (ii) Merchant's and Solm : $2\phi + \lambda - \alpha = \pi/2$ (m. $[69^\circ - 82^\circ$ for steel])
 (iii) Lee and Shafeer : $\phi + \lambda - \alpha = \pi/4$
 (iv) Stabler : $\phi + \lambda - \frac{\alpha}{2} = \pi/4$

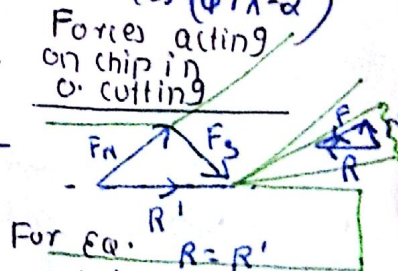
③ h, C_e, C_s, f $h = \max$ ht. of surface roughness $f = \text{mm}$ [Rev]

(i) $h_{\max} = \frac{f}{\cot C_e + \tan C_s}$ # surface finish puts limit on max. feed.
 (ii) $h_{\max} = \frac{f^2}{8r}$ (iii) $R_A = \frac{h_{\max}}{4}$ $R_A = \text{Avg. line of Roughness.}$

If $\uparrow r \rightarrow$ vibration, chattering, Force \uparrow , Power \uparrow
 # For smooth surface \rightarrow \downarrow feed, $\downarrow C_e, \uparrow C_s$
 # Tool Radius Provides \rightarrow Good surface finish, longer tool life

④ MERCHANT'S CIRCLE DIAGRAM $F_S = \frac{C_s \cdot t \cdot b}{\sin \phi}$ $F_C = F_S \cdot \cos(\lambda - \alpha)$

only depends on ϕ } Power = $F_C \cdot V = F_S \cdot \omega \cdot \frac{\cos(\lambda - \alpha)}{\cos(\phi + \lambda - \alpha)} = \frac{C_s \cdot t \cdot b \cdot \omega \cdot \cos(\lambda - \alpha)}{\sin \phi \cdot \cos(\phi + \lambda - \alpha)}$
 Specific cutting energy = $\frac{F_C}{bt} = \frac{M}{m^2} = \frac{1}{m^3}$
 F_C = cutting force = along cutting velocity
 F_T = Thrust force = normal to "



- ⑤ (i) Turning : For outer surface
 (ii) Boring : Enlarging of existing hole made by drilling or casting
 (iii) Counter-boring : To enlarge only a limited portion of hole
 (iv) Reaming : To " end of hole to give it conical shape for short distance
 (v) Tapping : To make internal threads using Tap.
 (vi) Reaming : Requiring dimensional accuracy and surface finish is obtained by multi-toothed Tool called Reamer.

⑥ $M \cdot C$ $\angle 2\theta$ $M \cdot \text{angle} = 2\theta$ $\uparrow \theta \rightarrow$ For Hard and Brittle } opp. to Rake
 $\downarrow \theta \rightarrow$ For soft " Ductile }

- ① GRINDING WHEEL SPECIFICATION (Mgn. code, A, G, G1S, B, Mgn code)
- A Type of Abrasive [Al_2O_3 , SiC, Diamond]
 - G Grain or Grit size [size of Abrasive particle] (fine, coarse)
 - G Strength of bond in wheel [Power of Abrasive particles] to hold together [soft, medium, hard]
 - S Structure [spacing b/w Abrasives] (Dense, open)
 - B Bond Type [V-vitrified, S-silicates, D-Diamond, B-Resinoid, E-Shellac]

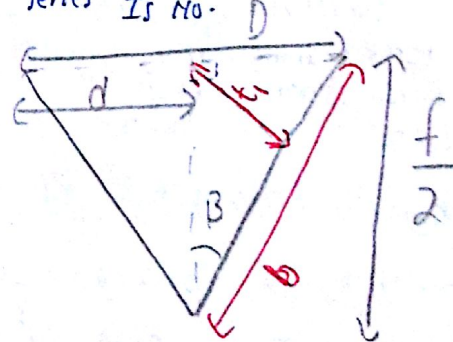
- ② (i) st. wheel \rightarrow only 1 grain size used.
 (ii) compound " \rightarrow >1 " " " "
- ③ coarse grain size : soft, ductile [open structure, hard wheel]
 fine " " : hard, brittle [Dense " , soft wheel]
- ④ (i) off-hand grinding: work in hand pressed against rotating G.W.
 (ii) surface " : To grind horizontal flat surface.

- ⑤ GRINDING DEFECTS
- (i) **GLAZING**: If work material is hard, grains wear out quickly and sharpness of cutting edge lost.
 - (ii) **LOADING**: When chips occupy voids b/w Abrasive grains.
- REMEDY: DRESSING** \rightarrow Reconditioning process to grind the grinding wheel itself.

① Drill specification Drill dia, Series, Material, I.S. No.

Series N \rightarrow for Normal LCS
 H \rightarrow " Hard materials.
 S \rightarrow " Soft and Tough.

E.g. $\frac{105}{\text{Dia}} \frac{H}{\text{Series}} \frac{1504}{\text{IS No.}}$



② m/c ing for Drill

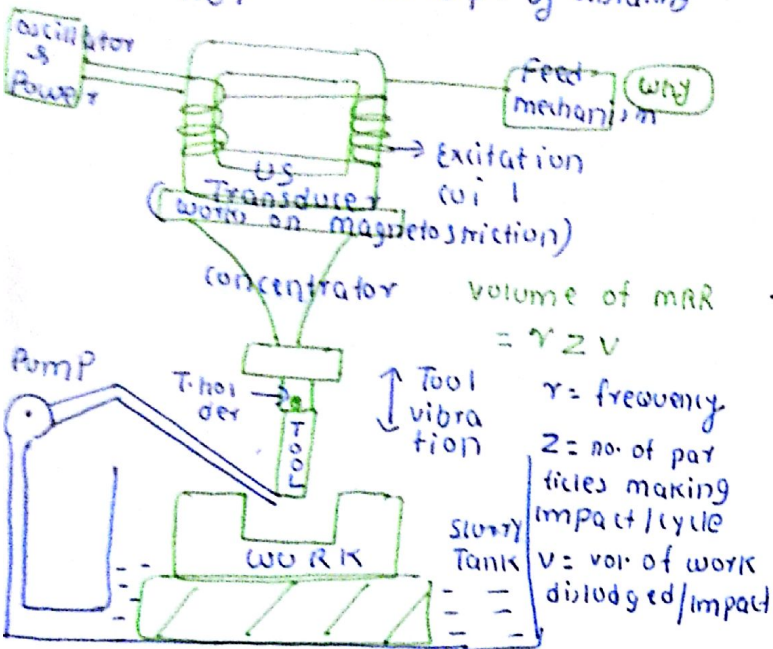
For 2 face $d = \frac{D}{2}$, $f = \frac{f}{2}$

For 3 face $d = \frac{D}{3}$, $f = \frac{f}{3}$

$$\rightarrow b = \frac{d}{\sin \beta} = \frac{D}{2 \sin \beta} \rightarrow t_1 = \frac{f}{2} \cdot \sin \beta \rightarrow v = \pi D N$$

\rightarrow $\text{Time} = \frac{L + 3D}{f N}$ \rightarrow Approach length.

USM: - Slurry of Abrasive grains hammered on w.p. by vibrating tool

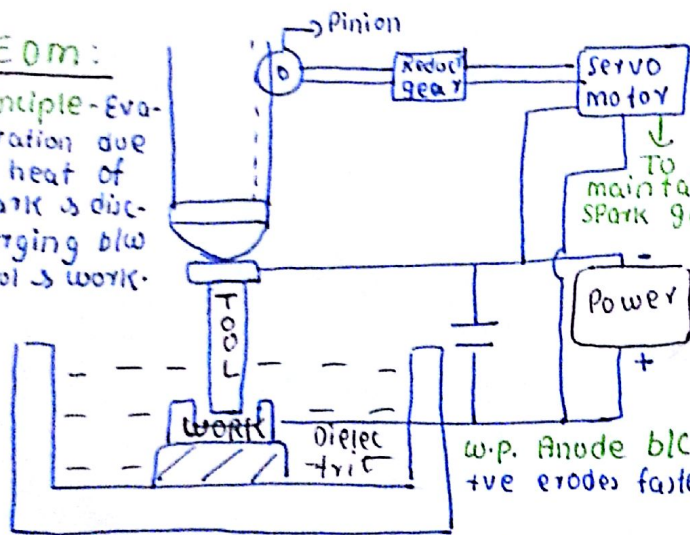


Volume of MRR = $\gamma Z V$

γ = frequency
 Z = no. of particles making impact/cycle
 V = vol of work dislodged/impact

ECM:

Principle - Evaporation due to heat of spark & discharging b/w tool & work.



DIELECTRIC

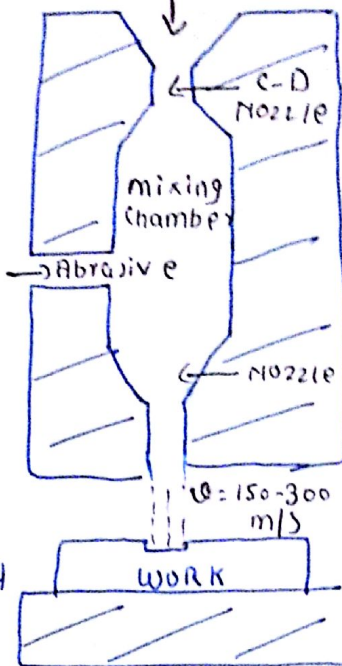
- 1- Drive away chips
 - 2- Res MRR
- * Viscosity, inflammable, cooling ability, chemically neutral
 - E.g. HC, some light oil, kerosene, paraffin oil

Tool wear:

W. Ratio = $\frac{\text{w.p. wear}}{\text{Tool wear}}$
 CI, brass, Cu, W, Ag, W

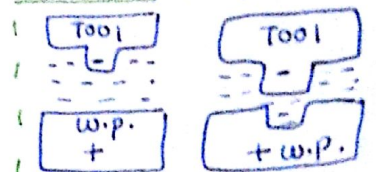
ATM

compressed air



Adv: Cheap, & power, & heat
 Disadv: & MRR, & sur. finish

Nozzles: subjected to wear
 Reverse of electroplating



- * Here no Tool wear
- * Use Tool, w.p. of same
- * Material from w.p. can add to Tool & change its shape → To prevent it electrolyte
- * Low voltage DC applied
- * Anodic dissolution Removes material from w.p.
- * Constant feed motion to Tool & electrolyte pumped at 1 pr.

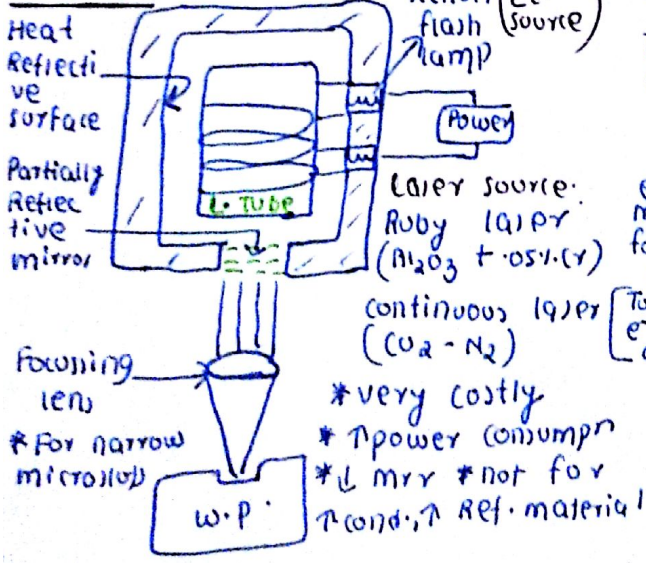
MRR: 10-15 times of EDM
 Power & sur. fin. & w.p. elec. conductor

Dielectric: salt soln
 Electrolyte: 1- complete E. fluid
 2- carry away heat & waste
 3- Allow EC React. xly.

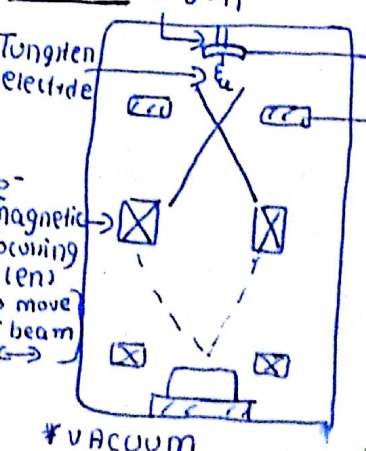
Properties: Elec., Thermal K, T.C.P., & vis., non corrosive, toxic
 * 20% NaCl in water, HCl in water, H₂SO₄ in water, HNO₃
 $\alpha = \frac{e_i}{F \cdot \text{valency}} \cdot \frac{\text{cm}^3}{\text{sec}}$ i = current (A)
 $e = 96500$
 $C = \frac{A}{Z} \cdot \frac{\text{At. wt.} \cdot \rho_m}{\text{valency}}$ F = F. cond
 Alloy: $\gamma, \alpha, \beta, \delta, \epsilon, \zeta, \eta, \theta, \iota, \kappa, \lambda, \mu, \nu, \xi, \omicron, \pi, \rho, \sigma, \tau, \upsilon, \phi, \chi, \psi, \omega, \pi, \rho, \sigma, \tau, \upsilon, \phi, \chi, \psi, \omega$
 $\frac{100}{e} = \sum \frac{x_i}{e_i} = Z$

PAM:

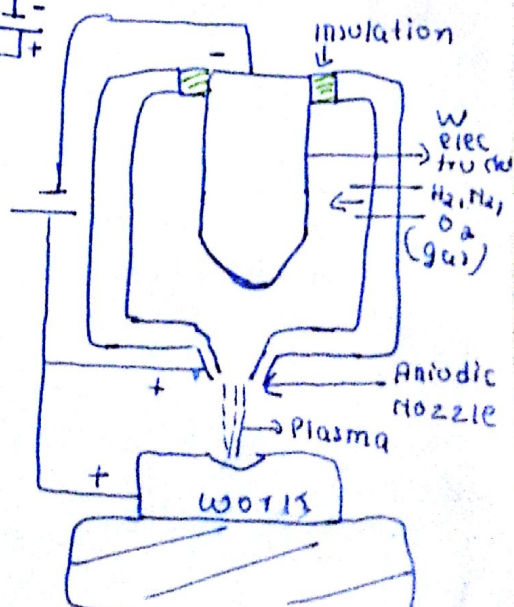
EBM:



EBM:



Plasma is a T ionised gas
 - for conductors



- (1) IN Arc welding the arc length should be : $4-5$ times the $r_{\text{electrode}}$
- (2) Cutting Tool Material Required to sustain \uparrow Temp: Cermet
- (3) Centrifugal casting: $\begin{cases} \text{Coarse grain size} \\ \text{High } \uparrow \text{ density} \end{cases}$
- (4) To Melt Non-Fe Alloys: Induction furnace
- (5) Symbol to indicate Roughness: $\sqrt{\text{ }}$
- (6) Follow board pattern: For castings having weak portions which may break due to Ramming.
- (7) In $V T^n$ n for Ceramic Tools: $.6 - .75$
- (8) " " " " Carbide " : $.2 - .4$
- (9) (i) Manual \rightarrow constant current I (Droop char)
(ii) Automatic \rightarrow " voltage V (St. line ")
- (10) AHW: Arc b/w 2 w electrode not b/w w.p. and electrode.
- (11) GEAR GENERATING PROCESS: (i) Hobbing
(ii) Gear shaper
(iii) Rack planing
- (12) Surface finish by Honing: $.01 \mu\text{m}$ (CLA).
- (13) Railway Tyres fitted by \rightarrow Interference fit
- (14) Laser Beam: No vacuum
e⁻ Beam: vacuum
- (15) Max. Reduction in tube drawing by: moving mandrel method.
- (16) To Extrude Brittle materials like Cu : Hydrostatic Extrusion.
- (17) (i) Bolt heads: upsetting [localised forging of work piece]
(ii) Hexagonal " " : closed die upsetting.
- (iii) Railway wheels: $\begin{cases} \text{Roll forging (Earlier)} \\ \text{Inv. casting (Now)} \end{cases}$
- (iv) a- Rifle barrel: Swagging.
b- gun : Gun drilling.
- (18) To manufacture Extrusion Nozzles: White Cast Iron.
- (19) GANG MILLING \rightarrow 2 or more cutters mounted on common arbor, used simultaneously

- ① Dry and compressed air is used for milling \rightarrow Cast Iron.
- ② Ideally single pt. Thread cutting Tool should have \rightarrow +ve Rake.
- ③ Rate of wear is pre-dominant in \rightarrow Tungsten Carbide (WC) Tools.
- ④ Internal gears can be made by \rightarrow Gear shaping with pinion cutter.
- ⑤ H-R Plane in Rolling:
 - (i) Velocity of Roll (not 60) = velocity of material
 - (ii) Friction force = 0 (Shear = 0)
 - (iii) Normal force $P = \max$.
- ⑥ For condition of Self Entry: $\tan \theta \leq \mu$ $\theta =$ Bite angle.
- ⑦ nip angle = 2μ (radians): it is the bite \angle at Rolling limit.

- ⑧ DEEP DRAWING
 - (i) curvature on die: (8-12) $\%$ (iii) clearance on die: (1.2-1.4) t
 - (ii) Shear on punch: (4-6) $\%$ (iv) pressure on Blank holder: 2% of $\frac{F}{A}$.

⑨ chip produced for brass = discontinuous

⑩ 18-4-1 : W, Cr, V.

⑪ sand casting \rightarrow can be used for ornamental parts.

⑫ up or conventional milling Down or climb milling



(i) direction work

opp. direcⁿ

(ii) Surface

poor

(iii) Tool life

low



same direcⁿ

good

High

⑬ shrinkage values: mm/m

white metal (5) Cast Iron (10)

Bronze (15)

Copper (16)


Aluminium (17) Brass (18)

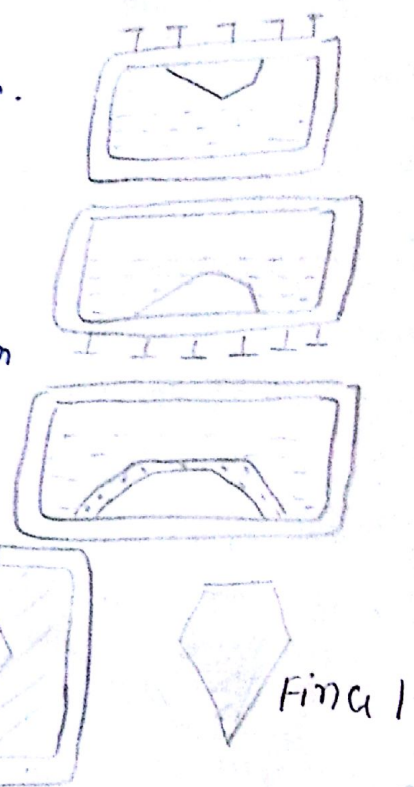
Steels (20)

Classification of casting

- | | | |
|-----------------------------|---|---------------------|
| (i) Expandable moulds | (ii) permanent moulds | (iii) continuous C. |
| A- SAND CASTING | A- CENTRIFUGAL C. | |
| B- SHELL " | B- DIE C. $\begin{cases} \text{Gravity} \\ \text{Pressure} \end{cases}$ | |
| C- INVESTMENT " | C- SLUSH C. | |
| D- CO ₂ moulding | | |
| E- Full moulding | | |

1) Shell moulding

- Better surface finish and close dimⁿ Tolerance.
- Pattern: CI, Al, Brass Heated to 230-315°C
- Pattern clamped in box having: **Silica, Alcohol, Phenolic Resin**
- Invert the box: Thickness of sand stick to pattern
- Dwell time: Time for forming
- Heat pattern + shell → Then take out the shell
- Join 2 shells → 
- FOR NON-FE METALS
- Thin section, Sharp corner, Small projection



2) Investment Casting

- $\begin{cases} \text{Wax} & \text{Pattern: LOST WAX PROCESS} \\ \text{Hg} & \text{MERCAST PROCESS} \end{cases}$
- CASTING OF: ↑ mt Pt. and ↑ strength Alloy
- (A) wax pattern ~~dipped~~ ^{Rinsed} in **Alcohol** (To Remove grease and dirt)
- (B) After drying pattern dipped in slurry [**Si flour, water, ethyl silicate**]
- On slurry Add some fine grain ceramic: (called **PRE COAT**)
- Turbine, Jet blades. (For Repetition of process)

- | | |
|---|--------------------------------------|
| Step 1 make wax pattern in die | } Steps Heat it to Remove wax |
| Step 2 form a tree of these patterns using central sprue | |
| Step 3 (A) Step 4 (B) Repeat it | |
| → layer of sand appear over it | |
| Step 5 Fire shell in furnace to complete Remove wax. | |
| Step 6 pour metal, solidity, break it, final product. | |

③ SODIUM SILICATE OR CO₂ MOULDING: [For Hard Mould]

- Hard mould: Better finish, dimn Tolerance
- Mix 3-4% Na_2SiO_3 with sand while preparing mould.
- $\text{P} \rightarrow \text{CO}_2$ $\text{Na}_2\text{SiO}_3 + \text{CO}_2 \rightarrow \text{Na}_2\text{CO}_3 + \text{SiO}_2$ (colloidal)
- Dis ad: ↓ Collapsibility

④ Full moulding or Lost Foam process:

Pattern: Plastic Polyesterene

Moulding Material: Gypsum or pop (∵ distortion while Ramming ∴ sand x)

When hot metal poured: (vaporises)

⑤ CENTRIFUGAL CASTING

Rotated: 3000 rpm

Poured: At centre

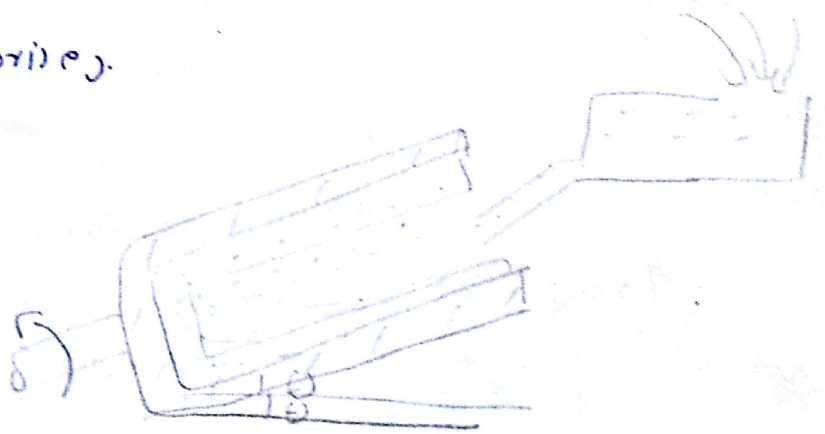
C.Y = 95-98%

outside grains → coarse

centre " → fine

Apply → large pipe, boiler, pressure vessels, flywheel, etc.

which have symmetry



Semi-centrifugal casting Placed on H.P., Rotated abt. vertical Axis

outer portions of mould by → centrifugal

central " " " → gravity

Apply → wheel, pulley.

Centrifuging No. of castings, individual gates, central sprue

Purpose: To force metal from a central Axis to individual mould cavities which are placed on circumference

Need not be Axis-symmetric

Application: patterns for Investment casting

⑥ Slush casting ↓ melting pt. material Brass Pb, Sn, Zn

Apply → Lamp shade, Toy, decorative item, Jewellery, Hollow castings with thin walls.

⑦ Continuous C Al, Cu ✓ Fe X

Numerical values for surface finish: 1- Peak to valley height: R_z (Limitation sudden Jerk)
 2- Distance b/w 7th peak, 1st valley - R_1, R_{max}, H_{max} (ii) Area $R_a = \frac{\sum a \sum b}{L}$
 3- centre line avg. value: $R_a = \frac{\sum y}{n}$ $L = \text{cut off length}$
 4- R_{ms} : $R_g = \sqrt{\frac{\sum y^2}{n}}$ * Approx $R_a = \frac{H_{max}}{4}$ $H_{max} = \frac{f^2}{8r}$ $H_{max} = \frac{f}{\cot \alpha + \tan \alpha}$
 5- 10 pt. value $R_2 = \text{Avg. of 5 next peaks \& 5 next valleys.}$

Representation of surface finish:

1- ∇ (8.25 μm) (1.6-8) (.025-1.6) (.025) (L/A)

TALY SURF:- measures surface irregularities

- Diamond pt. at end of lever
- Skid to protect D. pt.
- As D. pt. moves in valley position of core in coil changes
- Resistance changes
- use wheatstone bridge.

2-

- a) marking allowance
- b) Roughness value
- c) Direction of Lay
- d) Sampling/cut off L
- e) Production method

COMPARATORS:

- Relative Inspection - measures dimn from a Reference value
 - usually datum by slip gauges - don't move π distances to maintain π
 1- cheap 2- No ext. power supply 3- Accuracy Independent of A. in manufac-
 4- mag. factor limited to 1000 5- limited Range turing diff. links
 6- Insensitive to small changes in dimn due to inertia 7- usually it has linear scale.

(i) Sigma C - magnet

variation in size of w.p. \rightarrow m.c. \uparrow or \downarrow \rightarrow cylinder over Ribbon
 Rotates \rightarrow Deflection of pointer.
 # why D. spring is not helical? H.S. not used as Restoring device in measurement b/c it takes time to come back to new position.
 # C-slots in diaphragm spring: To Relieve any Residual stress in spring
 # magnet - To avoid any Jerk & maintain uniform pressure.

(ii) Mikrotak

Due to pivot movt. of m.c. \rightarrow movt. of Twisted spring
 # Thin metal strip: given LH Twist on L. side & RH Twist on R. side central portion neutral.
 # if w.p. size changes \rightarrow imbalance in R.H. & L.H. Twist \rightarrow Portion rotates
 Principle: of AIR JET.
 - If Δ led then P_b will \uparrow .

$L = \text{stand off distance}$ # popular in Indus-
 - In process gauging
 - m.f. \uparrow 50000
 - comp. air anyway used in industry

2- PNEUMATIC COMPARATORS:

(i) Flow Type of Rotameter:

Float with Aerofoil blades
 $P_2 = b.p.r.$
 $P_1 = \text{supply pressure}$
 working: due to $P_2 - P_1$ position of Rotameter will change
 # P_1, P_2 don't mix (inside/outside below)
 - based on below position from neutral can decide which one higher.

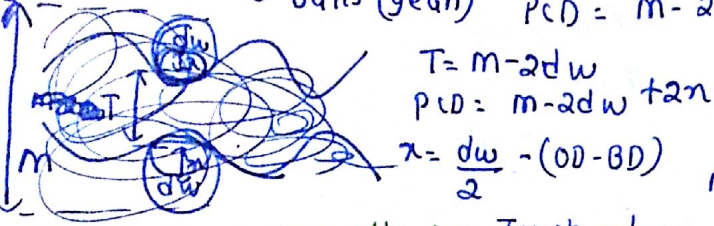
(ii) Differential type:

(iii) Back pressure type:

total pressure
 $d_c = \text{dia of control orifice}$
 $d_m = \text{dia of measuring orifice}$
 $M = \text{Area of measuring orifice} = \pi \cdot d_m \cdot l$
 $\frac{P_1}{P} = A - b \left\{ \frac{M}{C} \right\}$ (linear b/w $\frac{P_1}{P} = .6 \text{ to } .8$)
 Pneumatic sensitivity $\frac{dP_1}{dM} = .4 \frac{P}{M_{avg}}$ Indicators $S = \frac{dR}{dP_1}$
 m.h. sen = $\frac{dM}{d\Delta} = \pi d_m$

Screw Thread Metrology: major dia - ext. micrometer

minor dia - optical projector - TMM - pointed anvil micrometer
 Angle - " " pitch - pitch gauges - optical projector
 PCD - using wires 2 wire for pitch

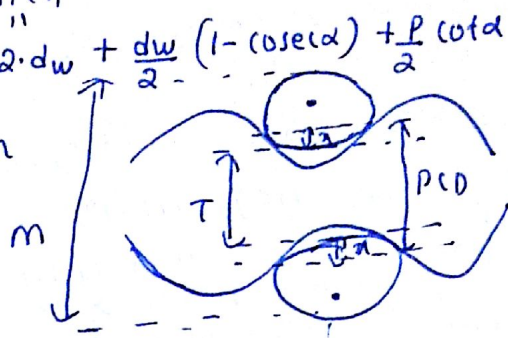


$$T = M - 2dw$$

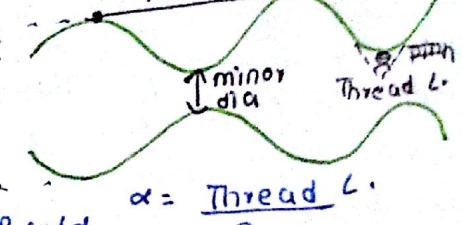
$$PCD = M - 2dw + 2n$$

$$n = \frac{dw}{2} - (OD - BD)$$

* For exact size dia i.e. Touch at pitch pt.
 $dw = \frac{P}{2} \cdot \sec \theta$



$$PCD = M - 2 \cdot dw + \frac{dw}{2} (1 - \cos \alpha) + \frac{P}{2} \cot \alpha$$

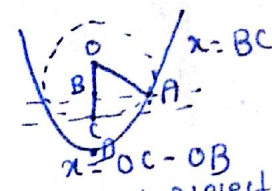


$$\alpha = \frac{\text{Thread } L}{2}$$

$$P = \text{pitch}$$

$$PCD = T + 2n$$

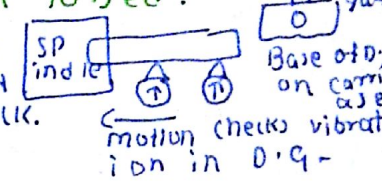
$$= M - 2 \cdot dw + 2n$$



Acceptance Test - on new m/c before inducn for mass production.

1- Dynamic: - on m/c in working condn - use std. condn - check product - if error - reject
 2- static: For 3 m/c's Lathe, milling, Drilling.

I For Lathe: (i) is bed True (use spirit level) (ii) is spindle axis || to bed:
 (iii) is Axis of work || to spindle axis: - use Reflector of Auto collimator



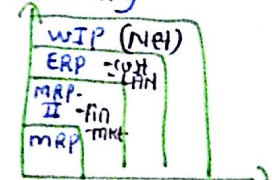
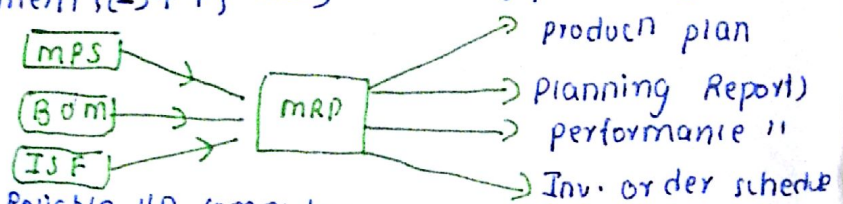
- use Reflector of Auto collimator - 2 sets of Reading on w.p. on head stock.

TQM: Initiated in Japan - what it is: orgn wide quality focussed culture.
 * A mgt. approach of orgn ^{centered on} quality ^{based on} participation of all members
 Aim: at long term success thru \rightarrow customer satisfaction
 Benefit to (i) orgn member (ii) society. Empowering

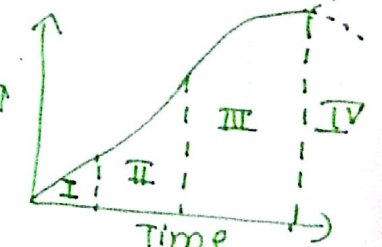
Some guiding principles: 1- Objective (continuous quality \uparrow) 2- Approach: Team work, staff
 3- scale (Everyone: orgn, supplier, customer) 4- Std. (do it Rt. the 1st time) 5- Measure (customer satisfaction)
 6- philosophy: prevention. 7 Tools: commitment, participation, motivation, edu, training.

Implementation:
 Elements: 1- customer orientation / satisfaction (multi dimⁿ) 2- Rt. 1st time
 3- continuous improvement 4- Employee involvement 5- Empower staff
 6- Benchmarking 7- Feedback
 Benefits: To 1- customer 2- company 3- staff.
 6 Phases of TQC: comprehension, commitment, competence, commⁿ, correctn, continuance
Ts control: 6. maintenance + 6. improvement {C \rightarrow + P} of various gyps in orgn.

MRP: material Requirement planning
 master product sch., Bill of material,
 Inv. status file * what it does * how it does
 * Benefits * limitations Assembly oriented, Reliable 1p, computers.
MRP-II: manufacturing Resource planning * MRP + financial + mktg
 (i) strategic P&C (ii) Tactical P&C (iii) Executive P&C
ERP: Enterprise Resource planning
WTP: web integrated planning (Buy + sell on net)



JIT: JAP - J Resource - on demand product - pull - difficult to handle Dy. - no Inv., S.S.
 - mail product - 10 workers - good vendor Reln.
Product life cycle: Introduce - growth - maturity - \rightarrow Rebirth / Death



Value: = Performance / funen / quality - cost value
 - Use " - Esteem " - Exchange "
 v. engg. \rightarrow Before product in mkt.
 v. Analysis \rightarrow After " " " BLAST \rightarrow CREATE \rightarrow REFINE.

PPC: PLANNING PHASE \rightarrow Action phase \rightarrow Control phase
 - Despatching
 Prior p. Active p.
 - Forecasting - order writing - Tool Control - Routing - scheduling
 - product design - material " - loading

Data collectn Interpr etation Expiditing Replan