

# 4.

## WELL HYDRAULICS

### SPECIFIC YIELD ( $S_y$ )

The specific yield of an unconfined aquifer is the ratio of volume of water which will flow under saturated condition due to gravity effect to the total volume of aquifer ( $v$ ).

$$S_y = \frac{V_{wy}}{V} \quad \text{where, } V_{wy} = \text{Volume of water yielded under gravity effect} \\ \text{and } V = \text{Total volume of water.}$$

### SPECIFIC RETENTION

The specific retention of an unconfined aquifer is the ratio of volume of water retained against gravity effect to the total volume of aquifer ( $v$ ).

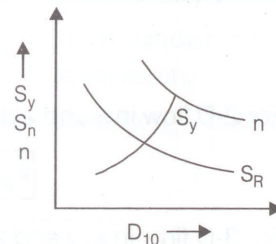
$$S_R = \frac{V_{WR}}{V} \quad \text{where, } V_{WR} = \text{Volume of water retained under gravity effect.}$$



**Remember**

$$S_y + S_R = n$$

where,  $n$  = Porosity

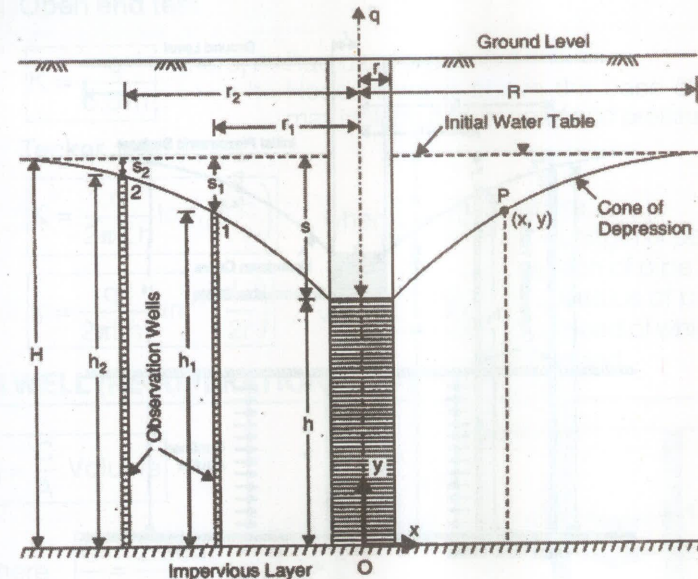


### COEFFICIENT OF TRANSMISSIBILITY

$$T = kH$$

where,  $H$  = Thickness  
 $k$  = Coefficient of permeability

## UNCONFINED AQUIFER



### (a) Theims Theory

$$q = \frac{k\pi}{2.303} \frac{(h_2^2 - h_1^2)}{\log_{10}(r_2/r_1)}$$

$$h_1 + s_1 = h_2 + s_2$$

$$\text{drawdown} = (h_2 - h_1) = s_1 - s_2$$

where,  $q$  = Rate of flow in  $m^3/s$   
 $h_1$  = Height of water table of 1<sup>st</sup> observation well  
 $h_2$  = Height of water table of 2<sup>nd</sup> observation well  
 $s_1$  = Drawdown of 1<sup>st</sup> test well  
 $s_2$  = Drawdown of 2<sup>nd</sup> test well.

$r_1$  and  $r_2$  are radius of 1<sup>st</sup> and 2<sup>nd</sup> observation wells respectively.

### (b) Dupits Theory

$$q = \frac{k\pi}{2.303} \frac{(H^2 - h^2)}{\log_{10}(R/r)}$$

$$R = 3000.S\sqrt{k} \quad \text{and}$$

$$S = H - h$$

Where,  $S$  = Drawdown in the well  
 $k$  = Permeability coefficient in  $m/s$ .

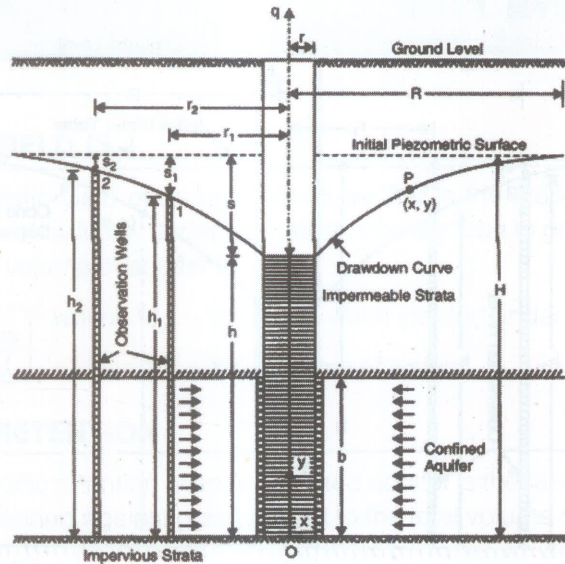
$R$  = Radius of influence in 'm'

$$150m \leq R \leq 300m$$

$r$  = Radius of test well in 'm'.

Results of dupits theory are not accurate because 'R' is based on empirical relation.

## CONFINED AQUIFER



(a) Theims theory  $q = \frac{2\pi bK(h_2 - h_1)}{2.303 \log_{10} \left( \frac{r_2}{r_1} \right)}$  where, b = width

(b) Dupits theory  $q = \frac{2\pi bK(H-h)}{2.303 \log_{10} \left( \frac{R}{r} \right)}$

## SPHERICAL FLOW THROUGH WELL

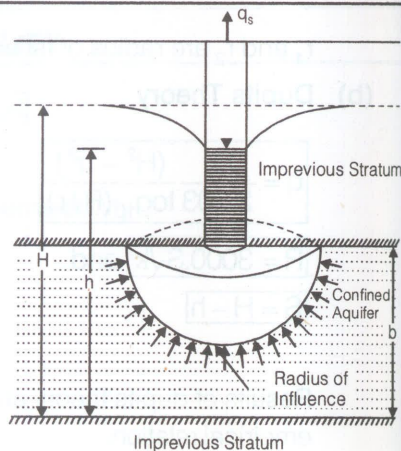
$$q_s = K \cdot 2\pi r \cdot s$$

where,  $r$  = Radius of well

S = Drawdown

$q_s$  = Rate of flow through spherical well in  $m^3/s$

$$q_s = \frac{1}{30} \cdot q_{\text{radial flow}}$$



## PUMPING-IN-TEST

(a) Open end test

$$K = \frac{q}{5.5rh} \quad \text{where, } r = \text{Radius of pipe}$$

h = Head of water above the base of pipe, it may include gravity head and pressure head.

(b) Tacker test

$$K = \frac{q}{2\pi Lh} \log_{10} \left( \frac{L}{r} \right) \quad \dots \text{ when } L > 10r$$

where,  
 L = Length of perforated section of pipe  
 r = Radius of pipe  
 h = Head of which water is added.

$$k = \frac{q}{2\pi Lh} \sin^{-1} \left( \frac{L}{2r} \right) \quad \dots \text{ when } L < 10r$$

$$k = \frac{q}{2\pi Lh} \sin^{-1}\left(\frac{L}{2r}\right) \quad \dots \text{when } L < 10r$$

### OPEN WELL (RECUPERATION TEST)

$$q = \frac{C}{A} \cdot \text{Volume}$$

where,  $\frac{C}{A} = \frac{2.303}{T} \log_{10} \left( \frac{h_1}{h_2} \right)$

$$\text{Volume} = A.H$$

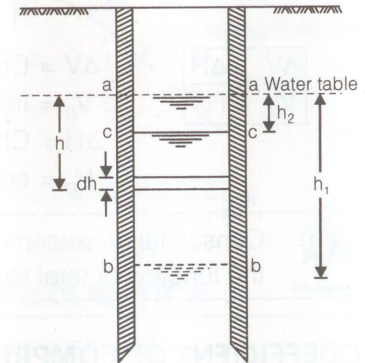
A = Area of well

$\frac{C}{A}$  = Specific yield or specific capacity of an open well.

T = Time in 'sec'

$h_1$  = Position of water table of  $t = 0$

$h_2$  = Position of water table of  $t = T$



### VALUES OF PERMEABILITY

	SOIL	K(cm/sec)	Degree of Permeability
1.	Coarse gravel	$>1$	High
2.	Fine gravel-Fine sand	$1 \text{ to } 10^{-2}$	Medium
3.	Silt-Sand admixtures, loose silts, rock flour and loess	$10^{-2} \text{ to } 10^{-4}$	Low
4.	Dense silt, clay silt admixtures, non-homogenous clays	$10^{-4} \text{ to } 10^{-6}$	Very low
5.	Homogenous clays	$<10^{-6}$	Impervious