

3. DESIGN & CONSTRUCTION OF GRAVITY DAMS

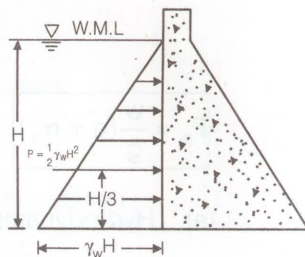
FORCES ACTING ON GRAVITY DAM

(i) Water Pressure

$$P = \frac{1}{2} \gamma_w H^2$$

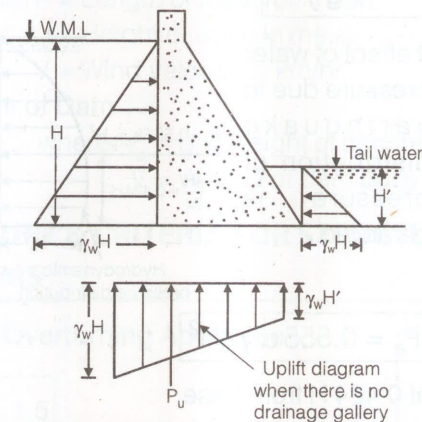
Acting at $\frac{H}{3}$ from base

where γ_w = Unit weight of water.

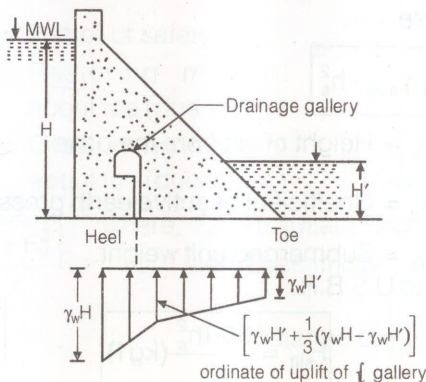


(ii) Uplift Pressure

(a) When Drainage Gallery is not Provided



(b) When Drainage Gallery is Provided



(iii) Earthquake Force

$$\alpha_H = 0.1g \text{ to } 0.2g \quad \text{where, } \alpha_H = \text{Horizontal acceleration}$$

$$\alpha_v = 0.75\alpha_H \quad \alpha_v = \text{Vertical acceleration}$$

$$\alpha = \beta I \alpha_0 \quad \alpha = \text{Seismic coefficient}$$

$$\beta = \text{Soil foundation system factor}$$

$$I = \text{Importance factor}$$

$$\alpha_0 = \text{Basic seismic coefficient which depends upon seismic zone of country.}$$

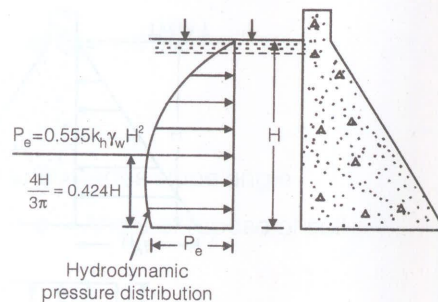
$$F_g = \frac{w}{g}(g \pm \alpha_v) \quad \text{where, } F_g = \text{Body force}$$

$$g = \text{Acceleration due to gravity, +ve for upward \& -ve for downward.}$$

(a) Hydrodynamic force

$$(i) F_H = \left(\frac{w}{g}\right) \alpha_H \quad F_H = \text{Horizontal Inertia force.}$$

(ii) It effect of water pressure due to earthquake distribution of pressure is parabolic.



$$P_e = 0.555 \alpha \gamma_w H^2$$

at $0.424 H$ from base.

$\alpha = 0.1g \text{ to } 0.2g$

(iv) Silt Pressure

$$F_{\text{silt}} = \frac{1}{2} k_a \gamma_{\text{sub}} \cdot h_s^2$$

where, h_s = Height of silt from the base.

$$k_a = \text{Coefficient of active earth pressure} = \frac{1 - \sin \phi}{1 + \sin \phi}$$

γ_{sub} = Submerged unit weight.

According to U.S.B.R

$$F_{\text{silt}} = \frac{360 h_s^2}{2} (\text{kg f})$$

(v) Wave Pressure

$$P_w = 2 \cdot 4 \gamma_w h_w$$

Acts at $\frac{hw}{8}$ from still water level.

where, P_w = Resultant wave pressure.

$$F_w = 2 \gamma_w h_w^2 \quad \text{acts at } \frac{3h}{8} \text{ from still water surface.}$$

where F_w = Total wave force.

$$h_w = 0.032 \sqrt{VF} + 0.763 - 0.271(F)^{3/4} \quad \text{if } F < 32 \text{ km.}$$

$$h_w = 0.032 \sqrt{VF} \quad \text{when } F > 32 \text{ km.}$$

where, F = Length of reservoir in km

h_w = Height of wave in meter

V = Wind velocity in km/hr.

(vi) Self Weight of Dam

$$w = \gamma_c V$$

where, γ_c = Unit weight of concrete

V = Volume of dam body per unit length

MODES OF FAILURE & CRITERIA FOR STRUCTURAL STABILITY OF GRAVITY DAMS

(i) Failure by Overturning About Toe

$$F_s = \frac{M_R}{M_o} > 1.5$$

where, F_s = Factor of safety

M_R = Restoring moment about toe (due to ΣF_v)

M_o = Overturning moment about toe (due to ΣF_H)

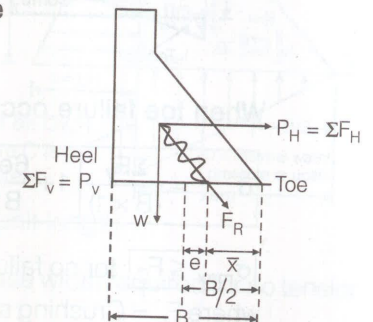
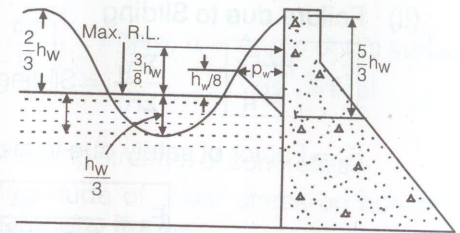
$$F_R = \sqrt{F_H^2 + F_V^2}$$

where, F_R = Resultant force

e = Eccentricity

$$e = \frac{B}{2} - \bar{x}$$

\bar{x} = Distance of $\vec{F_R}$ from toe.

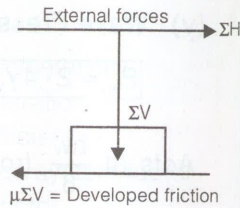


(ii) Failure due to Sliding

$$F_s = \frac{\mu \Sigma F_v}{\Sigma F_H} \quad \frac{\Sigma F_H}{\Sigma F_v} = \text{Sliding factor}$$

F_s = Factor of safety due to sliding.

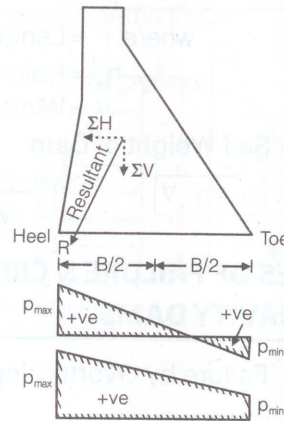
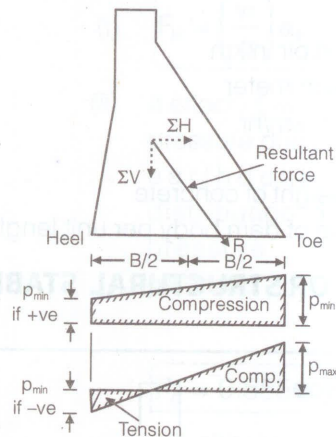
$$F_s = \frac{\mu}{\text{sliding factor}} > 1$$



Case : If shear strength is also accounted then factor of safety is called shear frictional factor (S.F.F)

$$S.F.F = \frac{\mu \Sigma F_v + q(B \times 1)}{\Sigma F_H} \quad [S.F.F > 3] \text{ where, } B = \text{Width in meter.}$$

(iii) Failure due to Compression or Crushing



When toe failure occurs.

$$\sigma_{\max} = \frac{\Sigma F_v}{(B \times 1)} \left[1 + \frac{6e}{B} \right]$$

When heel failure occurs.

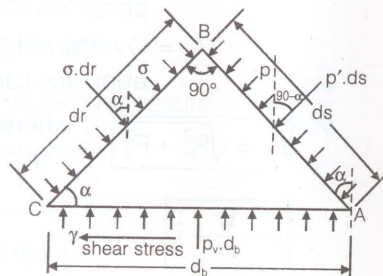
$$\sigma_{\min} = \frac{\Sigma F_v}{(B \times 1)} \left[1 - \frac{6e}{B} \right]$$

$$\sigma_{\max} \leq F_c \text{ for no failure}$$

where F_c = Crushing strength.

Case : (I) When shear stress also acts on horizontal plane.

$$\sigma_1 = \sigma_v \sec^2 \alpha - \sigma_2 \tan^2 \alpha$$



$$\sigma_v = \sigma_{\max} = \frac{\Sigma F_v}{(B \times 1)} \left[1 + \frac{6e}{B} \right] \quad \text{where, } \alpha = \text{Angle of d/s surface with vertical}$$

For no Failure,

$$\sigma_1 \leq F_c \quad \text{where, } F_c = \text{Crushing strength of concrete.}$$

$$\tau = \text{Magnitude of shear stress on horizontal plane near the toe.}$$

$$\tau = (\sigma_v - \sigma_2) \tan \alpha$$

Case (2): When earthquake force considered then

$$\sigma_1 = \sigma_v \sec^2 \alpha - (\sigma_2 - p_e) \tan^2 \alpha$$

$$\tau = [\sigma_v - (\sigma_2 - p_e)] \tan \alpha \quad \text{where, } P_e = \text{Earthquake Pressure.}$$

(iv) Failure due to Tension

$$\sigma_{\min} \geq 0 \rightarrow e \leq \frac{B}{6}$$

ELEMENTARY PROFILE OF GRAVITY DAM

$$\Sigma F_H = P_H = \frac{1}{2} \gamma_w H^2$$

$$P_u = \frac{1}{2} C \gamma_w H \cdot B$$

where P_u = Uplift pressure i.e., Force of buoyancy.

C = Uplift pressure coefficient.

$$w = \frac{1}{2} G \gamma_w \cdot B H$$

where w = Weight of dam body for unit length

$$B = \frac{H}{\sqrt{G - C}}$$

where, B = Minimum base width required for no tension criteria.

$$B' = \frac{H}{\mu(G - C)}$$

B' = Minimum base width for no sliding criteria.

G = Sp. gravity of concrete, i.e., that of the material of the dam

