

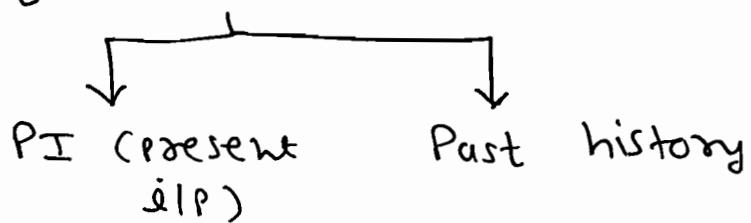


State

Space

Analysis:

\Rightarrow State \Rightarrow future behaviour



\Rightarrow The state gives the future behaviour of the sys. based on the present IIP & past history of the system.

\Rightarrow The past history (Initial condition) of the sys. described by the state Variable.

\Rightarrow The resistive ckt not having any state variable, because the o/p does not depends on the past history of the system.

\Rightarrow The resistive ckt o/p depends on only i/p.

\Rightarrow The resistive ckt cannot store any energy i.e. No past history, no state variables.

\Rightarrow The resistive ckt is called memoryless System.

* No. of State Variables:

⇒ If the RLC CKT given then the

no. of State Variable = sum of
Inductors & Capacitors.

⇒ If the differential eqⁿ is given,

No. of State Variable = Order of diffⁿ
eqⁿ.

* Standard form of State model:-

$$\begin{array}{c} \text{Diff}^n \rightarrow \dot{X} = AX + BU \rightarrow \text{state eq}^n | \text{ dynamic eq}^n \\ \text{state vector} \quad \downarrow \quad \downarrow \\ Y = CX + DU \rightarrow \text{o/p eq}^n \\ \downarrow \quad \downarrow \\ \text{o/p state vector} \quad \text{IIP vector} \end{array}$$

⇒ A → State matrix.

B → I/P matrix.

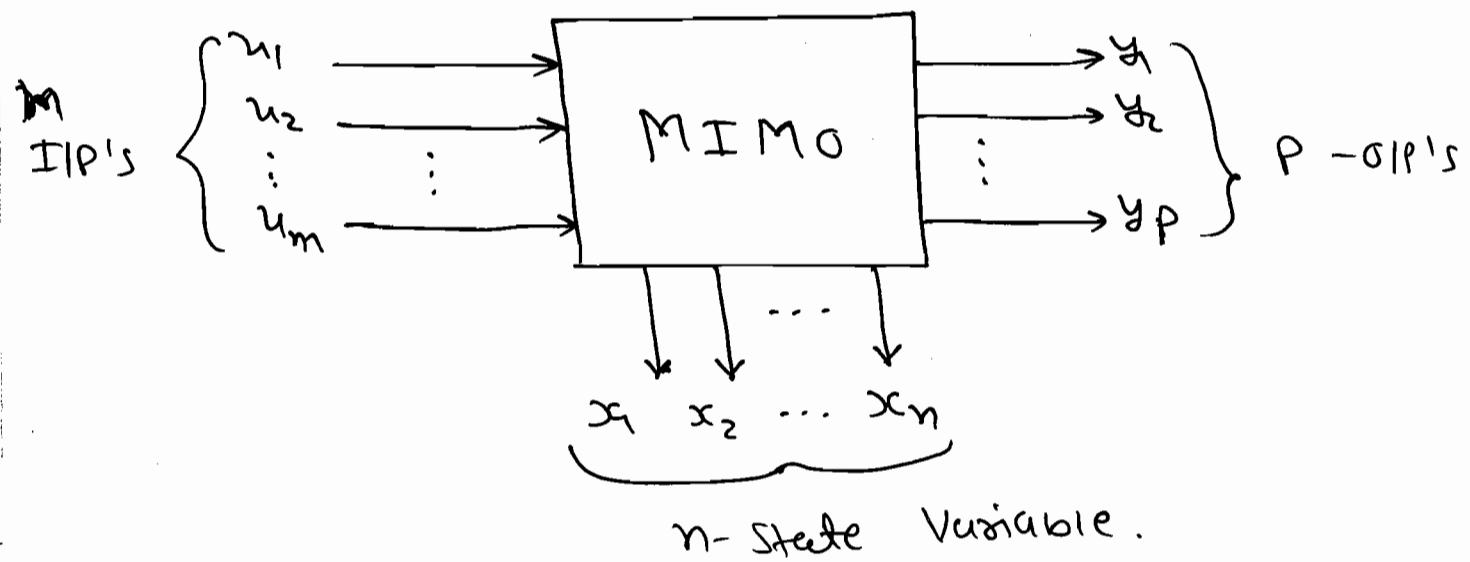
C → O/P matrix.

D → Transmission matrix.

* Order of Matrices:-

⇒ Consider the multi-I/P, multi O/P system as shown in fig.

\Rightarrow



$$\Rightarrow \text{I/P Vector } (u) = \begin{bmatrix} u_1 \\ u_2 \\ \vdots \\ u_m \end{bmatrix}_{m \times 1}$$

$$\Rightarrow \text{O/P Vector } (y) = \begin{bmatrix} y_1 \\ y_2 \\ \vdots \\ y_p \end{bmatrix}_{p \times 1}$$

$$\Rightarrow \text{State Vector } (x) = \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix}_{n \times 1}$$

$$\dot{x} = Ax + Bu$$

$\downarrow \quad \downarrow \quad \downarrow$
 $nx_1 \quad nx_1 \quad mx_1$
 $\downarrow \quad \downarrow$
 $nxn \quad nxm$

\Rightarrow The order of differential state vector must be equal to order of the state vector.

$$Y = CX + DU$$

↓ ↓ ↓
 $p \times 1$ $n \times 1$ $m \times 1$
 ↓ ↓ ↓
 $p \times n$ $p \times m$

* State Model to Differential eqn:-

Q] Write the state model to following systems:

① $\ddot{y} + 3\ddot{y} + 5\dot{y} + 7y = 10u$.

S.o.m: The No. of State Variable is 3, $n=3$

Let, $y = x_1 \quad \dots \quad ①$

$$\dot{x}_1 = \dot{y} = x_2 \quad \dots \quad ②$$

$$\dot{x}_2 = \ddot{y} = x_3 \quad \dots \quad ③$$

$$\dot{x}_3 = \ddot{y} = \dots \quad \dots \quad ④$$

\Rightarrow To get the x_3 in terms of state variables substitute all eqn in the given sys.

$$\therefore \dot{x}_3 + 3x_3 + 5x_2 + 7x_1 = 10u.$$

$$\Rightarrow \dot{x}_3 = -7x_1 - 5x_2 - 3x_3 + 10u \quad \dots \quad ⑤$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -7 & -5 & -3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 10 \end{bmatrix} [U].$$

$$[Y] = [1 \ 0 \ 0] \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

S.C.

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 & \dots \\ 0 & 0 & 1 & 0 & \dots \\ 0 & 0 & 0 & 1 & \dots \end{bmatrix}$$

Last row Coefficient from last to first with
opposite sign

⇒ The above State model is Controllable Canonical form. C CCF

⇒ The state models are not unique,
these are four types of state model.

① Controllable Canonical form.

② Observable Canonical form.

③ Diagonalization (or) Normal form.

④ Jordan Canonical form.

* Observable Canonical form:-

$$\Rightarrow A_{OCF} = (Acc_F)^T = \begin{bmatrix} 0 & 0 & -7 \\ 1 & 0 & -5 \\ 0 & 1 & -3 \end{bmatrix}$$

$$\Rightarrow B_{CCF} = \begin{bmatrix} b_0 \\ b_1 \\ b_2 \\ b_3 \end{bmatrix}_{\text{Start}}^{\text{End}} \Rightarrow B_{OCF} = \begin{bmatrix} b_3 \\ b_2 \\ b_1 \\ b_0 \end{bmatrix}_{\text{End}}^{\text{Start}}$$

$$\Rightarrow C_{CCF} \Rightarrow B_{OCF} = \begin{bmatrix} 10 \\ 0 \\ 0 \end{bmatrix}.$$

$$\Rightarrow C_{CCF} = [c_0 \ c_1 \ c_2 \ c_3], \quad \text{Start} \xrightarrow{\longrightarrow} \text{End}$$

$$C_{OCF} = [c_3 \ c_2 \ c_1 \ c_0] \quad \text{end} \xleftarrow{\longrightarrow} \text{Start}.$$

$$C_{OCF} = [0 \ 0 \ 1].$$

$$\boxed{Q} \quad \ddot{y} + 2\ddot{y} + 4\ddot{y} + 6y + 8y = 50.$$

Soln:

$$\dot{y} = x_1$$

$$\dot{x}_1 + 2x_4 + 4x_3 + 6x_2$$

$$\dot{x}_1 = \dot{y} = x_2$$

$$+ 8x_1 = 50.$$

$$\dot{x}_2 = \ddot{y} = x_3$$

$$\therefore \dot{x}_4 = -8x_1 - 6x_2 - 4x_3$$

$$\dot{x}_3 = \ddot{y} = x_4.$$

$$-2x_4 + 50.$$

$$\dot{x}_4 = \ddot{y} =$$

$$\therefore A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -8 & -6 & -4 & -2 \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 5 \end{bmatrix}, \quad C = [1 \ 0 \ 0 \ 0].$$

State model to the Transfer Function.

Q Write the State model to the given TF.

$$\frac{Y(s)}{U(s)} = \frac{2s+3}{s^2 + 5s + 6}$$

s^n :

$$\frac{Y(s)}{U(s)} = \frac{\dot{x}_1 = x_2 \quad 2s+3 \quad x_1}{s^2 + 5s + 6 \quad \downarrow \quad \downarrow \quad \text{②}}$$

$$\dots \quad \ddot{x}_1 = x_2 = s^3 \quad \dot{x}_2 \quad \ddot{x}_2 = x_2 \quad \text{①}$$

so, $\boxed{s^n = \dot{x}_n}$

$$\Rightarrow U = \dot{x}_2 + 5x_2 + 6x_1$$

$$\therefore \boxed{\dot{x}_2 = -6x_1 - 5x_2 + U} \quad \text{--- ②}$$

$$\Rightarrow Y = 2\dot{x}_1 + 3x_1$$

$$\boxed{Y = 2x_2 + 3x_1}$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & 1 \\ -6 & -5 \end{bmatrix}}_{\longrightarrow} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} [U].$$

$$[Y] = \underbrace{\begin{bmatrix} 2 & 3 \end{bmatrix}}_{\longrightarrow} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}.$$

Short-cuts:

$$\frac{Y(s)}{\rightarrow KU(s)} = \frac{K}{s^2 + ss + 6} \quad \begin{array}{l} \xleftarrow{\text{with same sign of}} \\ \xleftarrow{\text{co-effs.}} \end{array} \quad \begin{array}{l} \text{C matrix} \\ \text{A matrix} \end{array}$$

with opposite sign of coeffs.

Q) $\frac{Y(s)}{U(s)} = \frac{2s^3 + 4s^2 + 6}{s^5 + 3s^4 + 5s^3 + 7s^2 + 9s + 10}$

Soln:

$$\frac{Y(s)}{2U(s)} = \frac{-2(s^3 + 2s^2 + 3)}{s^5 + 3s^4 + 5s^3 + 7s^2 + 9s + 10}$$

$\downarrow \downarrow \downarrow \downarrow \downarrow \downarrow$

$x_5 \quad x_4 \quad x_3 \quad x_2 \quad x_1 \quad x_0$

A)

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 1 \\ -10 & -9 & -7 & -5 & -3 \end{bmatrix}$$

$$B = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 2 \end{bmatrix}$$

$$C = \begin{bmatrix} 3 & 0 & 2 & 1 & 0 \end{bmatrix}.$$

* Diagonalization form:-

$$\Rightarrow \frac{Y(s)}{U(s)} = \frac{1}{(s+1)(s+2)(s+3)}.$$

$$= \frac{Y_1}{s+1} - \frac{1}{(s+2)} + \frac{Y_2}{(s+3)}$$

$$\therefore Y = \frac{\frac{1}{2}U}{(S+1)} + \frac{-1U}{(S+2)} + \frac{Y_2 U}{(S+3)}$$

$$y = x_1 + x_2 + x_3.$$

$$\text{let, } x_1 = \frac{Y_2 U}{(S+1)}, \quad x_2 = \frac{-1U}{(S+2)}, \quad x_3 = \frac{Y_2 U}{(S+3)}$$

$$\Rightarrow Sx_1 + x_1 = \frac{1}{2}U$$

$$\therefore \dot{x}_1 + x_1 = \frac{1}{2}U$$

$$\boxed{\dot{x}_1 = -x_1 + \frac{1}{2}U} \quad - \quad ①$$

$$\Rightarrow Sx_2 + x_2 = -U.$$

$$\therefore \dot{x}_2 + x_2 = -U.$$

$$\Rightarrow \boxed{\dot{x}_2 = -x_2 - U.} \quad - \quad ②.$$

$$\Rightarrow Sx_3 + 3x_3 = \frac{1}{2}U.$$

$$\therefore \dot{x}_3 + 3x_3 = \frac{1}{2}U$$

$$\therefore \boxed{\dot{x}_3 = -3x_3 + \frac{1}{2}U.} \quad - \quad ③.$$

$$\therefore \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} -1 & 0 & 0 \\ 0 & -2 & 0 \\ 0 & 0 & -3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} \frac{1}{2} \\ -1 \\ Y_2 \end{bmatrix} [U].$$

↑ Poles (6s)
Eigen values.

Partial fraction

$$\Rightarrow [Y] = \begin{bmatrix} 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

Always 111...

\Rightarrow In the Diagonalization form B & C matrix are interchangeable.

* Jordan Canonical form:-

$$\Rightarrow \frac{Y(s)}{U(s)} = \frac{1}{(s+2)^2 (s+3)}$$

$$= \frac{1}{(s+2)^2} + \frac{-1}{(s+2)} + \frac{1}{s+3}.$$

$$\Rightarrow Y = \frac{1U}{(s+2)^2} + \frac{-1U}{(s+2)} + \frac{1U}{(s+3)}.$$

$$\Rightarrow Y = x_1 - x_2 + x_3.$$

where, $x_1 = \frac{U}{(s+2)^2} = \frac{U}{(s+2)} \cdot \frac{1}{(s+2)}$

$$\therefore x_1 = \frac{x_2}{(s+2)}.$$

$$\therefore sx_1 + 2x_1 = x_2.$$

$$\therefore \boxed{\dot{x}_1 = -2x_1 + x_2} \quad \text{--- (1)}$$

$$\Rightarrow x_2 = \frac{U}{(s+2)} \Rightarrow sx_2 + 2x_2 = U$$

$$\Rightarrow \boxed{\dot{x}_2 = -2x_2 + U.} \quad \text{--- (2)}$$

$$\Rightarrow x_3 = \frac{0}{s+3}.$$

$$\therefore 5x_3 + 3x_3 = 0.$$

$$\therefore \boxed{\dot{x}_3 = -3x_3 + 0} \quad \text{--- (3)}$$

Repeated Roots. i.e. Jordan block

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} -2 & 1 & 0 \\ 0 & -2 & 0 \\ 0 & 0 & -3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \\ 1 \end{bmatrix}$$

↑ zero's
↑ one's

$$[Y] = \begin{bmatrix} 1 & -1 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

↓ Partial fraction

Q) $\frac{Y}{U} = \frac{1}{(s+5)^3 (s+10)}.$

Soln:

$$A = \begin{bmatrix} -5 & 1 & 0 & 0 \\ 0 & -\frac{1}{5} & 1 & 0 \\ 0 & 0 & -\frac{1}{5} & 0 \\ 0 & 0 & 0 & -10 \end{bmatrix}$$

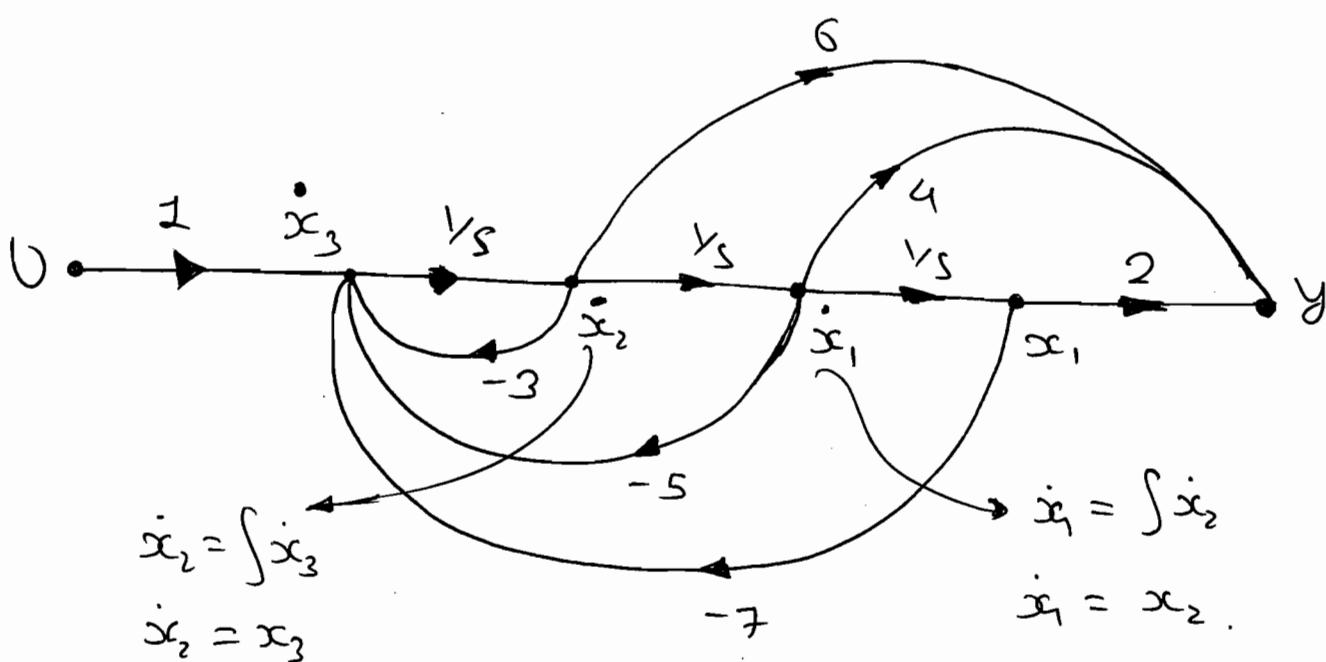
$$B = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 1 \end{bmatrix}, \quad C = \begin{bmatrix} k_1 & k_2 & k_3 & k_4 \end{bmatrix}$$

$\downarrow (s+5)^3 \quad \downarrow (s+5)^2 \quad \downarrow (s+5) \quad \downarrow (s+10)$

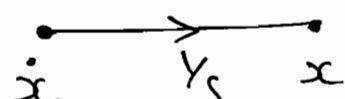
* State Model to the signal flow graph:

write the state model to the following signal flow graph.

Soln:



⇒ To select the node as a state variable, the incoming branch to that particular node must be a integrator, like



$$\Rightarrow \dot{x}_3 = 1 \cdot U - 3\dot{x}_2 - 5\dot{x}_1 - 7x_1.$$

$$\boxed{\dot{x}_3 = U - 3x_3 - 5x_2 - 7x_1}$$

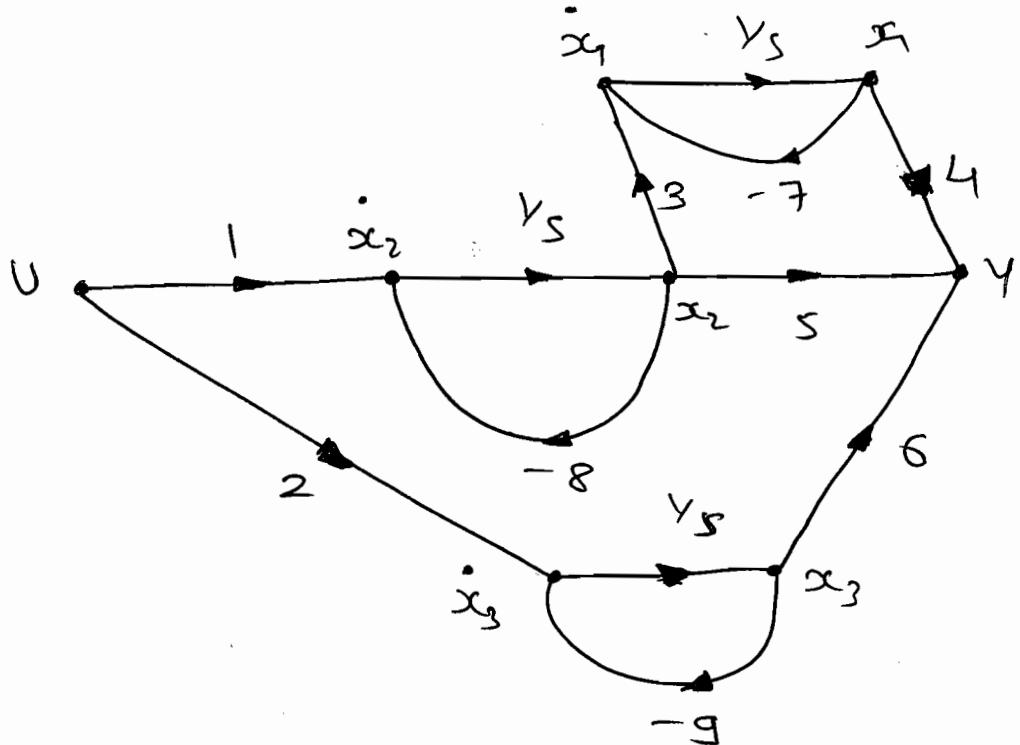
$$\therefore y = 2x_1 + 4x_2 + 6x_3$$

$$\boxed{\therefore y = 2x_1 + 4x_2 + 6x_3.}$$

$$\therefore \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -7 & -5 & -3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} [v].$$

$$[y] = [2 \ 4 \ 6] \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}.$$

a)



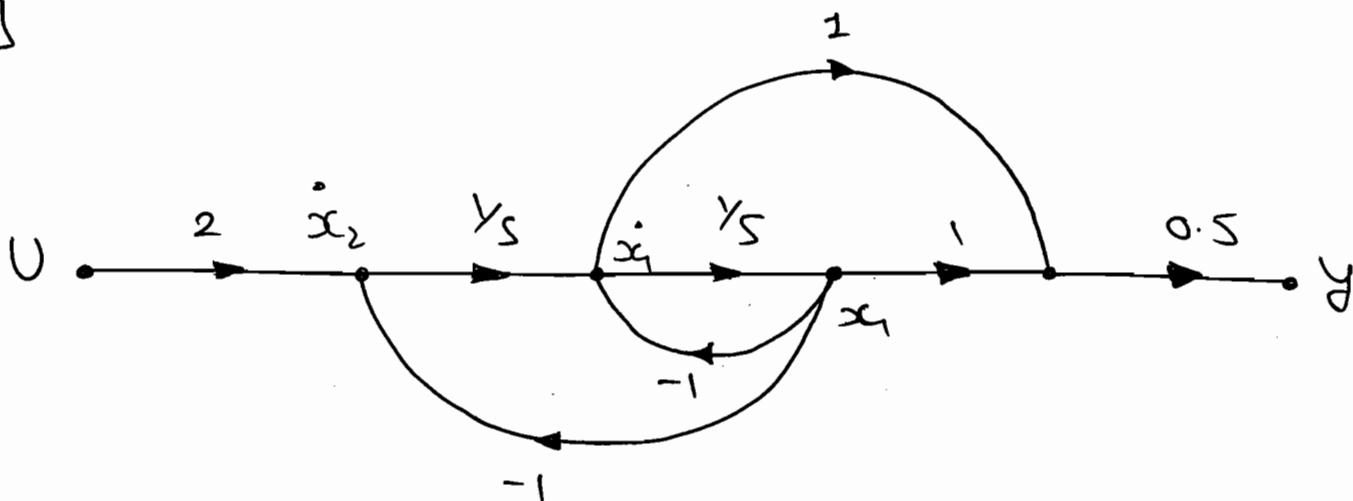
Soln:

$$\begin{aligned} \dot{x}_1 &= -7x_1 + 3x_2, \\ \dot{x}_2 &= -8x_2 + 2 \cdot 0, \quad y = 4x_1 + 5x_2 + 6x_3 \\ \dot{x}_3 &= -9x_3 + 2 \cdot 0. \end{aligned}$$

$$\therefore \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} -7 & 3 & 0 \\ 0 & -8 & 0 \\ 0 & 0 & -9 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \\ 2 \end{bmatrix} [v].$$

$$\therefore [y] = [4 \ 5 \ 6] \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

(a)



Soln:

$$\dot{x}_1 = \dot{x}_2 - x_1 = x_2 - x_1$$

$$\dot{x}_2 = 2u - x_1.$$

$$\therefore y = (x_1 + x_2) 0.5$$

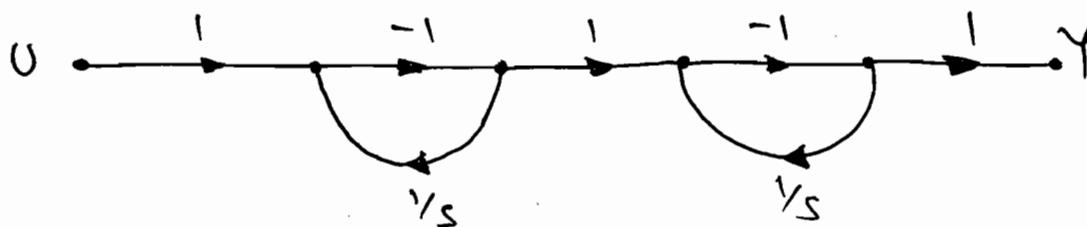
$$\therefore y = (x_2 - x_1 + x_1) 0.5$$

$$\therefore \boxed{y = 0.5\dot{x}_2}$$

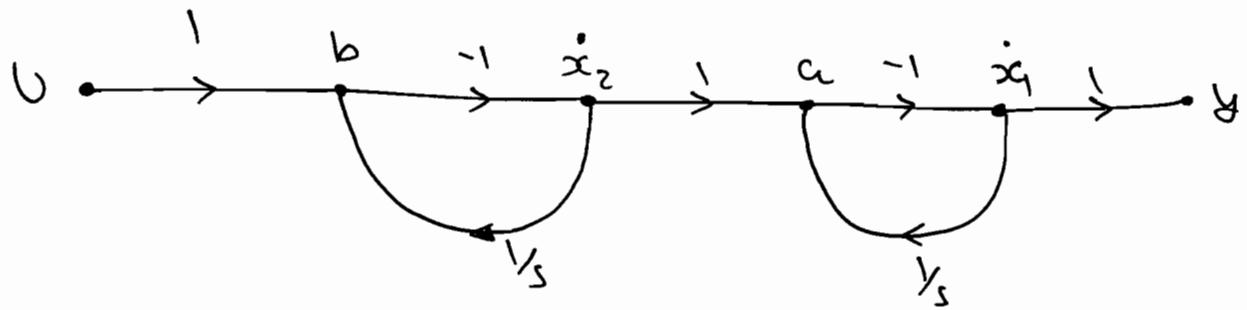
$$\therefore \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1 & 1 \\ -1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 2 \end{bmatrix} [u].$$

$$\therefore [y] = [0 \ 0.5] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}.$$

(b)



Sol'n:



$$\Rightarrow a = \dot{x}_2 + \frac{1}{s} \cdot x_1$$

$$a = \dot{x}_2 + x_1$$

$$\Rightarrow \cancel{\dot{x}_2} \neq b = J \cdot U + \dot{x}_2/s.$$

$$\therefore b = U + s x_2$$

$$\dot{x}_2 = -b$$

$$\boxed{\dot{x}_2 = -U - x_2.}$$

$$\dot{x}_1 = -a.$$

$$\therefore \dot{x}_1 = -x_1 - \dot{x}_2$$

$$\boxed{\dot{x}_1 = -x_1 + x_2 + U.}$$

$$y = \dot{x}_1$$

$$\boxed{y = -x_1 + x_2 + U.}$$

$$\Rightarrow \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ -1 \end{bmatrix} [U].$$

$$\therefore [y] = [-1 \quad 1] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + [1] [U].$$

 State model to the Electrical Nw:

\Rightarrow Select the state variables as
Voltage across Capacitors, and Current
through the conductors, Inductor.

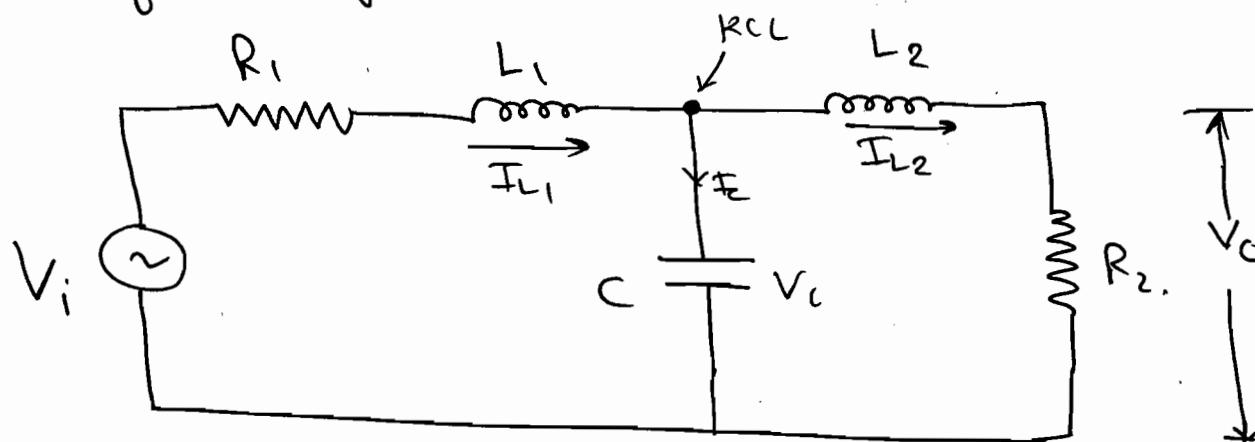
\Rightarrow The no. of state Variable $S =$ sum of Inductors & Capacitors.

\Rightarrow Write the independent KCL & KVL eqn.

\Rightarrow At Capacitor in apply KCL & apply KVL through the Inductor.

\Rightarrow The resultant eqn should consist, State Variables, differential State Variables, IIP Variables & o/p Variables.

Write the state model to the following system:



$$\text{Sol: } \text{SV (State Variable)} = \begin{bmatrix} V_c \\ I_{L1} \\ I_{L2} \end{bmatrix}$$

\Rightarrow KCL at Cap. jn

$$\therefore -I_{L1} + I_{L2} + C \frac{dV_c}{dt} = 0.$$

$$\therefore C \frac{dV_c}{dt} = I_{L1} - I_{L2}.$$

$$\dot{V}_c = \frac{I_{L_1}}{C} - \frac{I_{L_2}}{C} \quad - \textcircled{1}$$

$\rightarrow \underline{\underline{KVL_1}}$:

$$V_i - I_{L_1}R_1 - L_1 \frac{dI_{L_1}}{dt} - V_c = 0.$$

$$\therefore L_1 \frac{dI_{L_1}}{dt} = -I_{L_1}R_1 - V_c + V_i.$$

$$\therefore \dot{I}_{L_1} = -\frac{R_1}{L_1} \cdot I_{L_1} - \frac{V_c}{L_1} + \frac{V_i}{L_1} \quad - \textcircled{2}$$

$\rightarrow \underline{\underline{KVL_2}}$:

$$V_c - L_2 \frac{dI_{L_2}}{dt} - I_{L_2}R_2 = 0.$$

$$\therefore L_2 \frac{dI_{L_2}}{dt} = -I_{L_2}R_2 + V_c.$$

$$\therefore \frac{dI_{L_2}}{dt} = -\frac{R_2}{L_2} \cdot I_{L_2} + \frac{V_c}{L_2} \quad - \textcircled{3}$$

$$\Rightarrow \begin{bmatrix} \dot{V}_c \\ \dot{I}_{L_1} \\ \dot{I}_{L_2} \end{bmatrix} = \begin{bmatrix} 0 & \frac{1}{C} & -\frac{1}{C} \\ -\frac{1}{L_1} & \frac{-R_1}{L_1} & 0 \\ \frac{1}{L_2} & 0 & -\frac{R_2}{L_2} \end{bmatrix} \begin{bmatrix} V_c \\ I_{L_1} \\ I_{L_2} \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{L_1} \\ 0 \end{bmatrix} [V_i]$$

$$V_o = I_{L_2} \cdot R_2.$$

$$\therefore [V_o] = [0 \ 0 \ R_2] \begin{bmatrix} V_c \\ I_{L_1} \\ I_{L_2} \end{bmatrix}.$$

* Transfer function form the State

Model:

=>

$$T.F. = C [SI - A]^{-1} \cdot B + D.$$

$$T.F. = C \cdot \frac{\text{adj}[SI - A]}{|SI - A|} \cdot B + D.$$

=> The det of $SI - A$ i.e. $|SI - A| = 0$ gives the Chas. eqn.

=> The roots of the CE is called Poles which are called eigen values.

(e) find the T.F. to the given state model.

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -2 & -3 \\ 4 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 3 \\ 5 \end{bmatrix} [U].$$

$$[Y] = [1 \ 1] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}.$$

Sol'n: Add S diagonally & change the sign of coefficient to get $|SI - A|^{-1}$.

$$SI - A = \begin{bmatrix} S+2 & 3 \\ -4 & S-2 \end{bmatrix}.$$

$$\therefore (SI - A)^{-1} = \frac{\text{adj}(SI - A)}{|SI - A|} = \frac{\begin{bmatrix} S-2 & -3 \\ 4 & S+2 \end{bmatrix}}{S^2 - 4 + 12}.$$

$$\therefore T.F = C(CSI - A)^{-1} \cdot B + P.$$

$$= \frac{[1 \ 1]_{1 \times 2} \begin{bmatrix} s-2 & -3 \\ +4 & s+2 \end{bmatrix}_{2 \times 2} \begin{bmatrix} 3 \\ 5 \end{bmatrix}}{s^2 + 8}$$

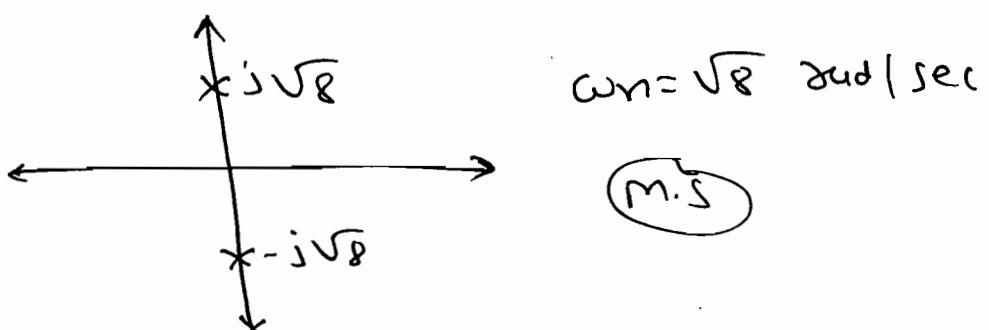
$$= \frac{[s+2 \ s-1] \begin{bmatrix} 3 \\ 5 \end{bmatrix}}{s^2 + 8}$$

$$= \frac{3s + 6 + 5s - 5}{s^2 + 8}$$

$$\boxed{TF = \frac{8s + 1}{s^2 + 8}}$$

$$\xrightarrow{CE} s^2 + 8 = 0 \Rightarrow s = \pm j\sqrt{8}$$

Marginaly stable (or) Undamped S.V.



(a) $\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 3 \\ -2 & -5 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 1 \end{bmatrix} [0].$

$$[y] = [2 \ 1] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}.$$

Sol'n:

$$SI - A = \begin{bmatrix} s & -3 \\ 2 & s+5 \end{bmatrix}.$$

$$(SI - A)^{-1} = \frac{\text{adj}(SI - A)}{|SI - A|}.$$

$$= \frac{\begin{bmatrix} s+5 & 3 \\ -2 & s \end{bmatrix}}{s^2 + 5s + 6}.$$

$$\therefore T.F. = C [SI - A]^{-1} B + D.$$

$$= \frac{[2 \ 1] \begin{bmatrix} s+5 & 3 \\ -2 & s \end{bmatrix} [1]}{s^2 + 5s + 6}$$

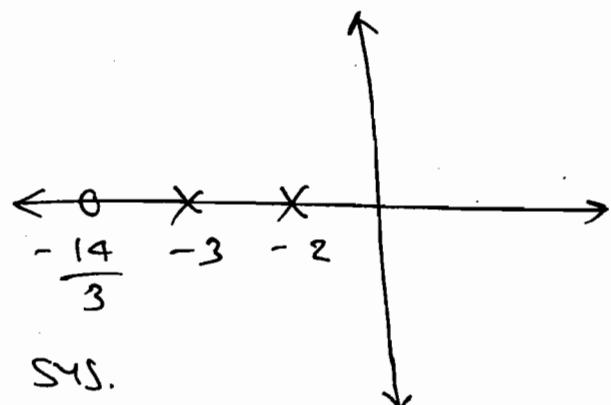
$$= \frac{[2s+8 \ 6+s] [1]}{s^2 + 5s + 6}$$

$$= \frac{2s+8 + 6+s}{s^2 + 5s + 6}.$$

T.F. = $\frac{3s+14}{s^2 + 5s + 6}$

Stable /

over-damped



* Solution to the State eqn:-

$$\Rightarrow \dot{X} = AX + BU \rightarrow \text{Non-Homogeneous State eqn.}$$

M-I : Laplace Transform method.

$$\Rightarrow SX(s) - X(0) = AX(s) + BU(s).$$

$$\therefore SX(s) - AX(s) = X(0) + BU(s).$$

$$\therefore (SI - A) X(s) = X(0) + BU(s).$$

$$\therefore X(s) = (SI - A)^{-1} X(0) + [SI - A]^{-1} \cdot BU(s).$$

⇒ Apply I.L.T.

$$\therefore x(t) = \mathcal{L}^{-1} \left\{ (SI - A)^{-1} X(0) \right\} + \mathcal{L}^{-1} \left\{ (SI - A)^{-1} BU(s) \right\}$$

Zero State Response due to I.C. -I
Zero Input Response due to I.P.

⇒ The zero IIP resp. (ZIR) is due to Initial Condition.

⇒ The zero State resp. (ZSR) is due to I.P.

M-II : Classical Method.

$$x(t) = e^{At} x(0) + \int_0^t e^{A(t-\tau)} \cdot B \cdot u(\tau) d\tau.$$

(II)

\Rightarrow Compute z_{IR} terms,

* *

$$\phi(t) = e^{At} = L^{-1} [S\mathbb{I} - A]^{-1}.$$

* *

STM: State Transmission matrix.

$$\Rightarrow [S\mathbb{I} - A]^{-1} = L[\phi(t)] = \phi(s).$$

$$\therefore \boxed{\phi(s) = [S\mathbb{I} - A]^{-1}}$$

\Rightarrow Compute z_{SR} term:-

$$\int_0^t \phi(t-\tau) B u(\tau) d\tau = L^{-1} [\phi(s) \cdot B \cdot u(s)].$$

$$\Rightarrow \boxed{x(t) = e^{At} \cdot x(0) + L^{-1} [\phi(s) \cdot B \cdot u(s)]} *$$

* *

* Properties of STM:-

$$\Rightarrow STM: \phi(t) = e^{At}.$$

$$\textcircled{1} \quad \phi(0) = e^0 = \mathbb{I} \quad (\text{Identity matrix}).$$

$$\textcircled{2} \quad \phi^k(t) = (e^{At})^k = A e^{A(kt)} = \phi(kt).$$

e.g. $\phi^{-1}(t) = \phi(-t).$

③ $\phi(t_1 + t_2) = \phi(t_1) \cdot \phi(t_2).$

④ $\phi(t_2 - t_1) \cdot \phi(t_1 - t_0) = \phi(t_2 - t_0).$

Q Obtain the Complete Sys. response of the system given below:

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ -2 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}, \quad x(0) = \begin{bmatrix} 1 \\ 1 \end{bmatrix}, \quad y = [1 \ -1] x.$$

Soln:

Homogenous State eqn:

$\dot{x} = Ax \rightarrow$ is called as homogenous State eqn. ($U=0$).

$$\rightarrow x(t) = \phi(t) \cdot x(0) = Z \cdot I \cdot R = e^{At} \cdot x(0).$$

$$x(t) = \phi(t) \cdot x(0)$$

$$\Rightarrow x(t) = L^{-1} [(S\mathbf{I} - A)^{-1} x(0)].$$

$$x(t) = L^{-1} [(S\mathbf{I} - A)^{-1} \cdot x(0)]$$

\Rightarrow The given state model is homogeneous
Hence the soln is

$$x(t) = Z \cdot I \cdot R = e^{At} \cdot x(0) = \phi(t) \cdot x(0).$$

$$\Rightarrow \xrightarrow{\text{STA}} \phi(t) = e^{At} = L^{-1} [S\mathbf{I} - A]^{-1}.$$

$$\phi(t) = L^{-1} [(sI - A)^{-1}]$$

$$\Rightarrow (sI - A) = \begin{bmatrix} s & -1 \\ 2 & +s \end{bmatrix}$$

$$\Rightarrow (sI - A)^{-1} = \frac{\text{adj}(sI - A)}{|sI - A|}$$

$$(sI - A)^{-1} = \frac{\begin{bmatrix} s & +1 \\ -2 & s \end{bmatrix}}{s^2 + 2}$$

$$\therefore \phi(t) = L^{-1} \begin{bmatrix} \frac{s}{s^2 + 2} & \frac{1}{s^2 + 2} \\ \frac{-2}{s^2 + 2} & \frac{s}{s^2 + 2} \end{bmatrix}$$

$$\therefore \phi(t) = \begin{bmatrix} \cos\sqrt{2}t & \frac{1}{\sqrt{2}} \sin\sqrt{2}t \\ -\sqrt{2} \sin\sqrt{2}t & \cos\sqrt{2}t \end{bmatrix}$$

$$\rightarrow x(t) = ZIR = \phi(t) \cdot X(0)$$

$$= \begin{bmatrix} \cos\sqrt{2}t & \frac{1}{\sqrt{2}} \sin\sqrt{2}t \\ -\sqrt{2} \sin\sqrt{2}t & \cos\sqrt{2}t \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix}_{2 \times 2} \begin{bmatrix} 1 \\ 0 \end{bmatrix}_{2 \times 1}$$

$$x(t) = \begin{bmatrix} \cos\sqrt{2}t + \frac{1}{\sqrt{2}} \sin\sqrt{2}t \\ \sqrt{2} \sin\sqrt{2}t + \cos\sqrt{2}t \end{bmatrix} \begin{bmatrix} -\sqrt{2} \sin\sqrt{2}t \\ + \cos\sqrt{2}t \end{bmatrix}$$

\Rightarrow The Complete Time Response is called $y(t)$.

→ Substitute x in y .

$$\therefore y(t) = \begin{bmatrix} 1 & -1 \end{bmatrix} \begin{bmatrix} \cos\sqrt{2}t + \frac{1}{\sqrt{2}}\sin\sqrt{2}t \\ -\sqrt{2}\sin\sqrt{2}t + \cos\sqrt{2}t \end{bmatrix}.$$

$$\therefore y(t) = \cancel{\cos\sqrt{2}t} + \frac{1}{\sqrt{2}}\sin\sqrt{2}t + \sqrt{2}\sin\sqrt{2}t - \cancel{\cos\sqrt{2}t}.$$

$$\therefore y(t) = \frac{3}{\sqrt{2}}\sin\sqrt{2}t.$$

(c) obtain the time response for unit - step IIP for a sys. given by.

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix}x + \begin{bmatrix} 0 \\ 5 \end{bmatrix}[0]$$

$$x[0] = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, y = [0 \ 1]x.$$

Soln:

$$x(t) = \phi(t)x(0) + L^{-1} \left[\phi(s) \cdot B U(s) \right].$$

$$\Rightarrow \phi(t) = L^{-1} \left[(sI - A)^{-1} \right].$$

⇒ The given state model is non-homogeneous. Hence, soln is

$$x(t) = Z \cdot I.R. + Z \cdot S.R.$$

$$\Rightarrow \xrightarrow{Z \cdot I.R.} e^{At} \cdot x(0) \Rightarrow \phi(t) \cdot x(0).$$

$$\Rightarrow \phi(t) = L^{-1} \left[(sI - A)^{-1} \right].$$

$$\therefore sI - A = \begin{bmatrix} s & -1 \\ -2 & s+3 \end{bmatrix}.$$

$$(sI - A)^{-1} = \frac{\text{adj}(sI - A)}{|sI - A|}.$$

$$= \frac{\begin{bmatrix} s+3 & +1 \\ -2 & s \end{bmatrix}}{s^2 + 3s + 2}.$$

$$= \frac{\begin{bmatrix} s+3 & +1 \\ -2 & s \end{bmatrix}}{(s+2)(s+1)}.$$

$$\therefore \phi(t) = L^{-1} \left[\begin{array}{c} \frac{(s+3)}{(s+2)(s+1)} & \frac{1}{(s+2)(s+1)} \\ \hline -2 & \frac{s}{(s+2)(s+1)} \end{array} \right]$$

~~After~~

$$\phi(t) = L^{-1} \begin{bmatrix} \frac{2}{s+1} - \frac{1}{s+2} & \frac{1}{s+1} - \frac{1}{s+2} \\ \hline -\frac{2}{(s+1)} + \frac{2}{s+2} & -\frac{1}{s+1} + \frac{2}{s+2} \end{bmatrix}$$

=

$$\phi(t) = \begin{bmatrix} 2e^{-t} - e^{-2t} & e^{-t} - e^{-2t} \\ -2e^{-t} + 2e^{-2t} & -e^{-t} + 2e^{-2t} \end{bmatrix}$$

$$\Rightarrow Z\text{-I.R.} = \phi(t) \cdot x(0).$$

$$= \begin{bmatrix} 2e^{-t} - e^{-2t} & e^{-t} - e^{-2t} \\ -2e^{-t} + 2e^{-2t} & -e^{-t} + 2e^{-2t} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix}.$$

$$\therefore Z\text{-I.R.} = \phi(t) \cdot x(0).$$

$$= \begin{bmatrix} 2e^{-t} - e^{-2t} \\ -2e^{-t} + 2e^{-2t} \end{bmatrix}.$$

$$\Rightarrow Z_{SR} = L^{-1} [\phi(s) \cdot B_U(s)].$$

$$= L^{-1} \begin{bmatrix} \frac{s+3}{(s+1)(s+2)} & \frac{1}{(s+1)(s+2)} \\ \frac{-2}{(s+1)(s+2)} & \frac{s}{(s+1)(s+2)} \end{bmatrix} \begin{bmatrix} 0 \\ 5 \end{bmatrix} \begin{bmatrix} 1 \\ s \end{bmatrix}$$

$$= L^{-1} \begin{bmatrix} \frac{s+3}{(s+1)(s+2)} & \frac{1}{(s+1)(s+2)} \\ \frac{-2}{(s+1)(s+2)} & \frac{s}{(s+1)(s+2)} \end{bmatrix} \begin{bmatrix} 0 \\ 5/s \end{bmatrix}$$

$$= L^{-1} \begin{bmatrix} \frac{5}{s(s+1)(s+2)} \\ \frac{5}{(s+1)(s+2)} \end{bmatrix}$$

$$= L^{-1} \left[\frac{5}{2s} - \frac{5}{s+1} + \frac{5}{2(s+2)} \right]$$

$$= L^{-1} \left[\frac{5}{(s+1)} - \frac{5}{s+2} \right]$$

$$= \left[\frac{s}{2} - s\bar{e}^{-t} + \frac{s}{2} \cdot \bar{e}^{-2t} \right]$$

$$\underbrace{s\bar{e}^{-t} - s\bar{e}^{-2t}}_{ZSR}$$

$$\rightarrow x(t) = ZFR + ZSR.$$

$$\Rightarrow x(t) = \left[\frac{5}{2} - 3\bar{e}^{-t} + \frac{3}{2} \bar{e}^{-2t} \right]$$

$$3\bar{e}^{-t} + -3\bar{e}^{-2t}$$

$$\Rightarrow y = [0 \ 1] x(t).$$

$$y(t) = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} \frac{5}{2} - 3\bar{e}^{-t} + \frac{3}{2} \bar{e}^{-2t} \\ 3\bar{e}^{-t} - 3\bar{e}^{-2t} \end{bmatrix}$$

\therefore

$$y(t) = 3\bar{e}^{-t} - 3\bar{e}^{-2t}$$

* Controllability & Observability :-

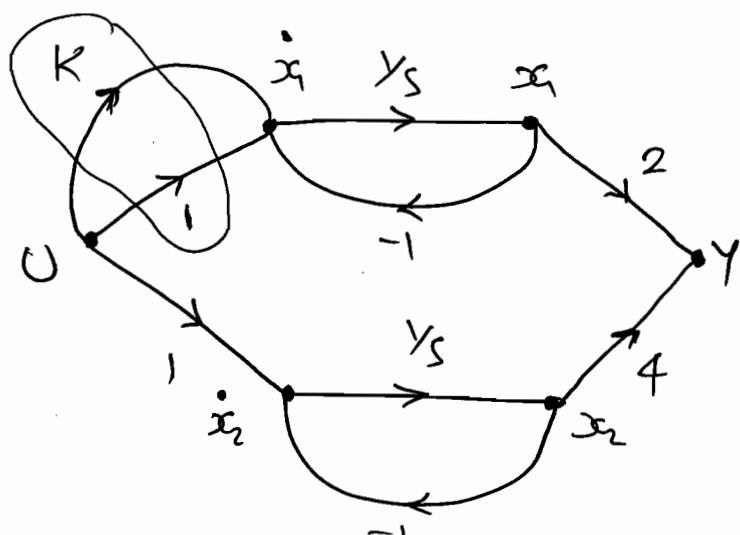
① Controllability :-

⇒ A sys. is ~~possible~~ Said to be Controllable if it is possible to transform the initial states to the desired state in a finite time interval by the controlled I/P.

⇒ If the SFG is given to check the Controllability observe the continuous path from I/P to each & every state variable.

⇒ If the Path is exist then it is called Controllable.

(a) Find the K value to become the system uncontrollable.



Soln: To become the system uncontrollable
no path exist betⁿ the u to x

$$\rightarrow K+1 = 0 \Rightarrow \boxed{K=-1}$$

* Kalman's test for Controllability (\mathcal{Q}_c):-

$$\Rightarrow \mathcal{Q}_c = [B \ AB \ A^2B \ \dots \ A^{n-1}B]$$

Controllable

$$\Rightarrow \begin{array}{l} \text{Rank of } \mathcal{Q}_c = \text{Rank of } A \\ |\mathcal{Q}_c| \neq 0 \end{array}$$

Check the Controllability to the given system.

$$\frac{Y(s)}{U(s)} = \frac{1}{s^3 + 2s^2 + 3s + 4}$$

Soln:
 $A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -4 & -3 & -2 \end{bmatrix}, B = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$.

$$\Rightarrow \mathcal{Q}_c = \begin{bmatrix} B & AB & A^2B \\ 0 & 0 & 1 \\ 0 & 1 & -2 \\ 1 & -2 & +1 \end{bmatrix} \Rightarrow |\mathcal{Q}_c| = 1 \neq 0$$

so, Controllable.

② Observability:

⇒ A sys. is said to be observable if it is possible to determine the initial states of the sys. by observing the op. in a finite time interval.

* Kalman's test for observability:-

$$\Rightarrow Q_0 = \begin{bmatrix} C^T & A^T C^T & (A^T)^2 \cdot C^T & \dots & (A^T)^{n-1} \cdot C^T \end{bmatrix}.$$

$$Q_0 = \begin{bmatrix} C \\ CA \\ CA^2 \\ \vdots \\ CA^{n-1} \end{bmatrix}$$

Observability

$\text{Rank of } Q_0 = \text{Rank of } A$ $ Q_0 \neq 0$

(a) Check the Controllability & observability for the following:-

System. $\dot{x} = \begin{bmatrix} 2 & 0 \\ -1 & 1 \end{bmatrix}x + \begin{bmatrix} 1 \\ -1 \end{bmatrix}u$.

$$A = \begin{bmatrix} 1 & 1 \end{bmatrix} X$$

Soln:

$$\Omega_C = \left[\begin{array}{cc} A & AB \\ C & CA \end{array} \right] \Rightarrow \Omega_C = \begin{bmatrix} B & AB \\ C & CA \end{bmatrix}$$

$$\Rightarrow \Omega_C = \begin{bmatrix} 1 & 2 \\ -1 & -2 \end{bmatrix}$$

$$|\Omega_C| = -2 + 2 = 0 \Rightarrow \text{Not Controllable.}$$

$$\Rightarrow \Omega_O = \begin{bmatrix} C \\ CA \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix}$$

$$\therefore |\Omega_O| = 1 - 1 = 0 \Rightarrow \text{Not observable.}$$

Q $\dot{x}_1 = -2x_1 + x_2 + u.$

$$\dot{x}_2 = -x_2 + u.$$

$$y = x_1 + x_2.$$

Soln:

$$A = \begin{bmatrix} -2 & 1 \\ 0 & -1 \end{bmatrix}, \quad B = \begin{bmatrix} 1 \\ 1 \end{bmatrix}.$$

$$C = \begin{bmatrix} 1 & 1 \end{bmatrix}.$$

$$\rightarrow \Omega_C = \begin{bmatrix} A & AB \\ 1 & -1 \\ 1 & -1 \end{bmatrix} \Rightarrow |\Omega_C| = 0$$

$$\Rightarrow \text{Not Controllable.}$$

$$\Rightarrow \mathcal{O}_d = \begin{bmatrix} C \\ CA \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 1 \\ -2 & 0 \end{bmatrix}$$

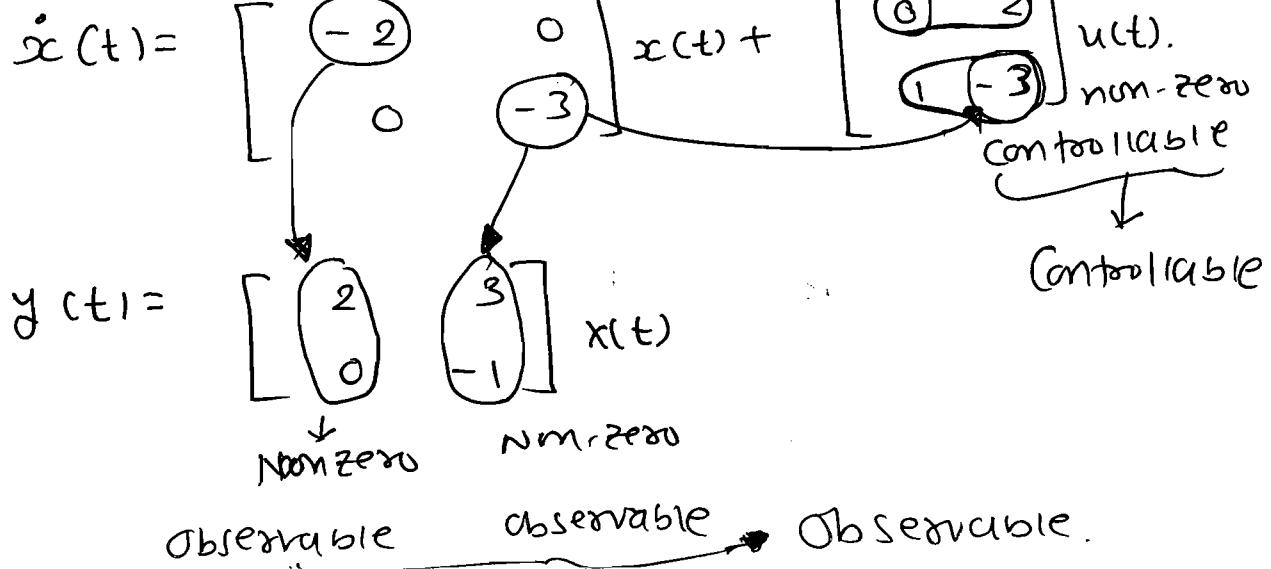
$\therefore |\mathcal{O}_d| = 2 \Rightarrow$ Observable.

\Rightarrow The Pole-Zero cancellation makes the system un-controllable & un-observable (or) Controllable & unobservable (or) uncontrollable & observable.

* Gibson test for Controllability & observability.

\Rightarrow The Gibson test is valid for only diagonalization form & Jordan Canonical form.

e.g.



\Rightarrow So, the given system is both observable and controllable.

e.g.

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} -2 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 1 & 0 & 0 \\ 0 & 2 & 0 \\ 0 & 0 & -3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 2 \\ 3 \end{bmatrix} u.$$

Jordan block.

$[y] = \begin{bmatrix} 1 \\ 0 \\ 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$

Non-zero
Non-zero
 \therefore observable
non-zero
non-zero
observable.
Observable.

Controlable
non-zero

\Rightarrow So, Sys. is controllable & observable.