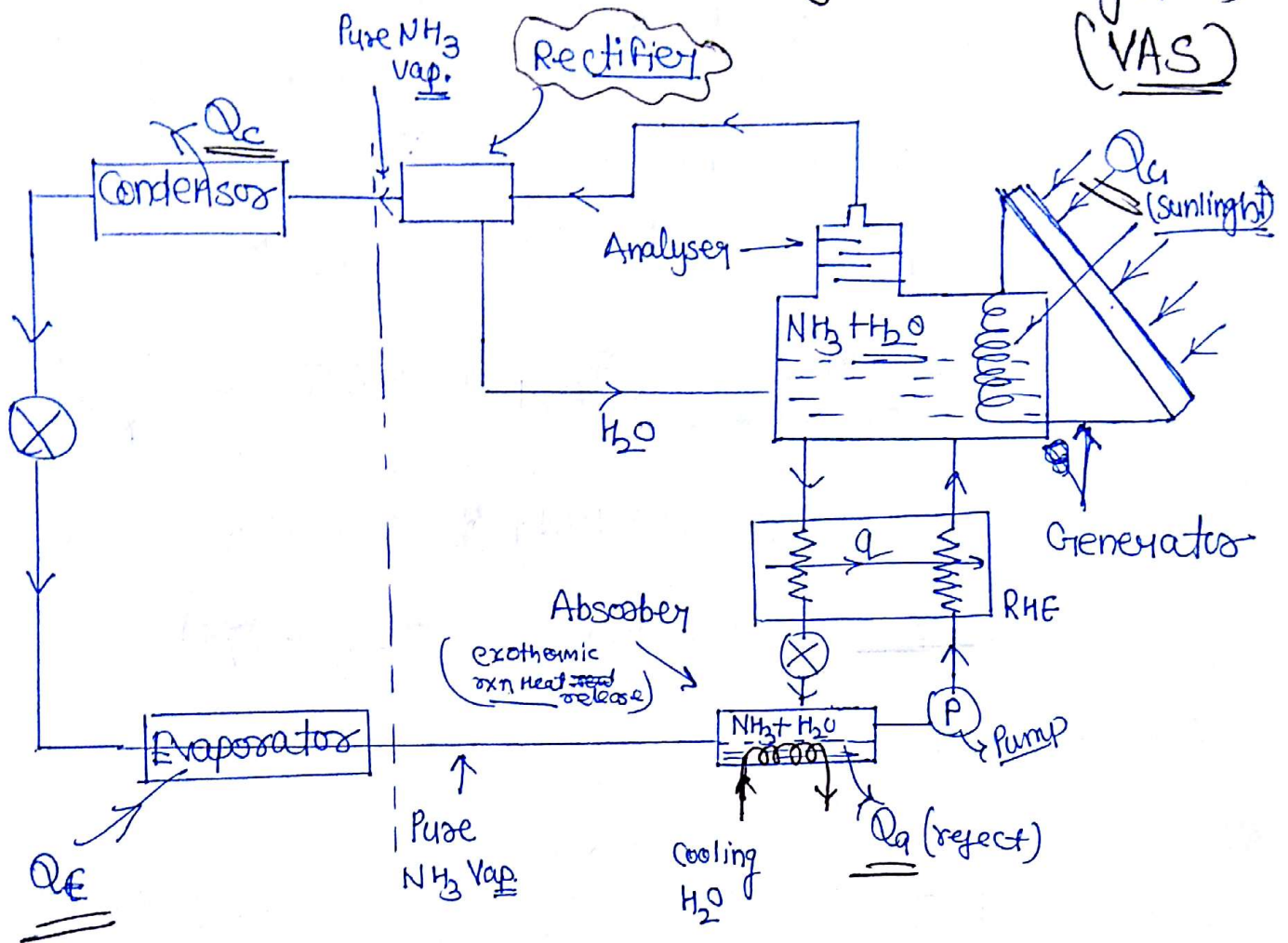


* Vapour Absorption Refrigeration System (VAS)



→ Pure NH_3 Vapour enters the absorber where it is absorbed in water (H_2O). The reaction is exothermic and the solubility of NH_3 is inversely proportional to temp. of solution. Cooling water is continuously circulating to maintain a low temp of solution to facilitate absorption of NH_3 . Solution rich in NH_3 is pumped to Generator via Regenerative heat exchanger. In Generator this solution absorbs heat and NH_3 separates.

forming high pressure NH_3 vapour.

- In RHE solution absorbs some heat from the water moving towards absorber. This reduces the need for heat absorption in generator.
- High pressure NH_3 vapour is passed through analyser where water vapour condenses. for complete removal of water vapour present with NH_3 vapour rectifier is installed.
- * Water vapour is presence is undesirable because it may freeze at the exit of the throttling ~~or~~ valve because of low temp. thus chocking the system.

* Important points.

- ① VAS works on low grade energy (Heat) whereas VCRS works on high grade energy (work).
hence COP of VAS is very less (0.3 to 0.5).
- ② Most popular VAS is $\text{NH}_3 - \text{H}_2\text{O}$ system. In this H_2O water is absorbent and NH_3 is refrigerant.
Other popular system are $\text{H}_2\text{O} - \text{LiCl}$ & $\text{H}_2\text{O} - \text{LiBr}$. In these two water is the refrigerant hence used for Air Conditioning purpose.

- ③ VAS are used where large waste heat is available or the cost of electricity is very high. Solar refrigeration system and Geothermal refrigeration system are based on VAS.
- ④ Heat is absorbed in generator and evaporator and heat is rejected in condensor & absorber.
- ⑤ Electrolux Refrigeration system is a VAS. It is three fluid system. ($\text{NH}_3 - \text{H}_2\text{O} - \text{H}_2$).
- ⑥ $\rightarrow$ Here NH_3 is the refrigerant, H_2O is absorbent and H_2 is used to create low partial pressure of NH_3 .
- ⑦ $\rightarrow$ No pump is used in this system and the fluid flows under the action of gravity due to density difference.

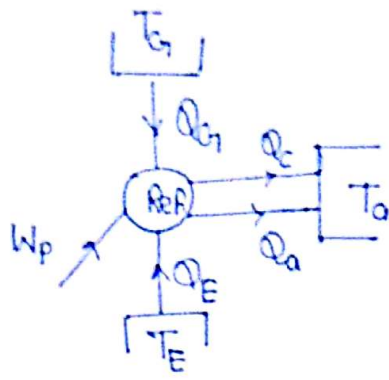
$$\text{COP} = \frac{Q_{\text{Evaporator}}}{Q_G + W_P}$$

$$Q_G \gg W_P$$

$$\boxed{\text{COP} = \frac{Q_E}{Q_G}}$$

For $(\text{COP})_{\text{max}}$

Refrigerator — Reversible.



energy consv.

$$Q_{G1} + Q_E + W_P = Q_c + Q_a$$

neglecting W_P

$$\Rightarrow Q_{G1} + Q_E = Q_c + Q_a \quad \text{--- (1)}$$

and law $\Rightarrow \oint_{\text{rev.}} \frac{dQ}{T} = 0$

$$\Rightarrow \frac{Q_{G1}}{T_{G1}} + \frac{Q_E}{T_E} - \frac{Q_c + Q_a}{T_0} = 0 \quad \text{--- (2)}$$

from eqⁿ (1) & (2)

$$\frac{Q_{G1}}{T_{G1}} + \frac{Q_E}{T_E} - \frac{Q_{G1} + Q_E}{T_0} = 0$$

$$Q_E \left[\frac{1}{T_E} - \frac{1}{T_0} \right] = Q_{G1} \left[\frac{1}{T_0} - \frac{1}{T_{G1}} \right]$$

$$Q_E \left[\frac{T_0 - T_E}{T_0 T_E} \right] = Q_{G1} \left[\frac{T_{G1} - T_0}{T_0 T_{G1}} \right]$$

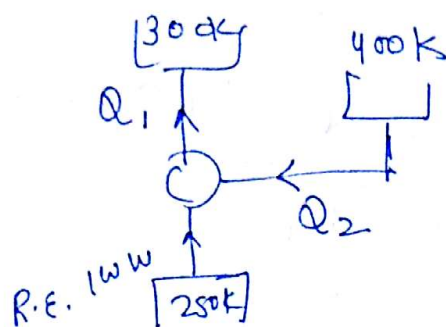
$$\frac{Q_E}{Q_{G1}} = \frac{T_E (T_{G1} - T_0)}{T_{G1} (T_0 - T_E)}$$

$$\star \boxed{(\text{COP})_{\text{max}} = \frac{T_E (T_{G1} - T_0)}{T_{G1} (T_0 - T_E)}}$$

P.9.49

Q.13

WB



$$\frac{Q_1}{300} = \frac{Q_2}{400} + \frac{2}{5}$$

$$Q_1 = 100 + Q_2$$

$$\frac{100 + Q_2}{300} = \frac{Q_2}{400} + \frac{2}{5}$$

$$\frac{1}{3} + \frac{Q_2}{300} = \frac{Q_2}{400} + \frac{2}{5}$$

$$\frac{1}{3} - \frac{2}{5} = Q_2 \left(\frac{400 - 300}{400 \times 300} \right)$$

$$\frac{5 - 6}{15} = Q_2 \frac{100}{120000}$$

$$\text{rej. } Q_2 = -80\text{W}$$

(T1)

$$T_H = 360\text{K}$$

$$T_0 = 310\text{K}$$

$$T_E = 260 \rightarrow 250\text{K}$$

$$\text{COP} = \frac{T_E(T_H - T_0)}{T_H(T_0 - T_E)}$$

$$\text{COP} = \frac{260(360 - 310)}{360(310 - 250)} = \frac{250(T_H - 310)}{T_H(310 - 250)}$$

$$\frac{13}{18} = \frac{250 T_H - 250 \times 310}{T_H \times 310 - T_H \times 250}$$

$$T_H = 374.9\text{K}$$

$$(12) \quad \text{COP} = \frac{T_E (T_G - T_0)}{T_G (T_0 - T_E)} =$$

$$\text{COP} = \frac{258 (383 - 328)}{383 (328 - 258)} = 0.529$$

$$(11) \quad \text{COP} = \frac{270 (360 - 300)}{360 (300 - 270)} = \frac{270 \times 60}{360 \times 30}$$

$$\text{COP} = 1.5$$

Ques In $\text{NH}_3\text{-H}_2\text{O}$ absorption system heat is supplied to generator by Condensing steam at 0.2 MPa. The initial state of steam is at a dryness fraction of 0.9 and the final state of the steam after Condensing is Saturated liquid. The temp. to be maintained in evaporator is -10°C and the surrounding temp is 30°C . (i) Find $(\text{COP})_{\text{max}}$

(ii) If the actual COP is 40% of max COP and refrigeration load is 20 TR, what will be the required steam flow rate (kg/s)

at 0.2 MPa $T_{\text{sat.}} = 120.2^\circ\text{C}$ $h_{fg} = 2201.9 \frac{\text{kJ}}{\text{kg}}$.

Soln

$$\begin{aligned}
 (COP)_{max} &= \frac{T_E (T_G - T_0)}{T_G (T_0 - T_E)} \\
 &= \frac{263 (128.2 - 30)}{393.2 (30 + 10)}
 \end{aligned}$$

$$(COP)_{max} = 1.508$$

$$R.E. = RE \times \dot{m}$$

~~$$20 \times 3.51 = (h_1 - h_4) \times \dot{m}$$~~

$$(COP)_{act} = 0.4 (COP)_{max}$$

$$\textcircled{1} \frac{RE}{W_{1/p}} = 0.4 \times 1.508 = 0.603$$

~~$$RE = 42.34 = \dot{m} (h_1 - h_4)$$~~

~~$$42.34 = \dot{m} (h_f + x h_{fg} - h_f)$$~~

~~$$\dot{m} =$$~~

$$\frac{RC}{\dot{Q}_a} = 0.603 = \frac{20 \times 3.5167}{\dot{m} \times x \times h_{fg}}$$

$$\dot{m} = 0.058 \text{ kg/s}$$