

HYDRAULICS TEST 3

Number of Questions: 25

Time: 60 min.

Directions for questions 1 to 25: Select the correct alternative from the given choices.

1. In a fluid the velocity field is given by

$$V = (3x + 2y)i + (2z + 3x^2)j + (2t - 3z)k$$
 The velocity at point (1, 1, 1) at time 2 second is
 (A) 6.82 units (B) 7.14 units
 (C) 7.93 units (D) 8.26 units

Statement for Linked Answer Questions 2 and 3:

The velocity along the centre line of a nozzle of length ℓ is given by,

$$V = 2t \left(1 - \frac{x}{2\ell} \right)^2$$

where V = velocity in m/s, t = time in seconds,
 x = distance from inlet of the nozzle

2. Convective acceleration when $x = 1$ m and $\ell = 1.5$ m and $t = 5$ seconds is
 (A) -19.75 m/s^2 (B) 19.75 m/s^2
 (C) 26.35 m/s^2 (D) -26.35 m/s^2
3. Total acceleration for the same conditions as above is
 (A) 20.64 m/s^2 (B) -20.64 m/s^2
 (C) -18.86 m/s^2 (D) 18.86 m/s^2
4. Velocity distribution in the boundary layer of fluid flow over a surface is given by

$$\frac{u}{U} = \frac{3}{2} \frac{y}{\delta} - \frac{1}{2} \frac{y^2}{\delta^2}$$

When δ = the boundary layer thickness
 U = maximum velocity of fluid
 u = fluid velocity at y

The ratio of displacement thickness to boundary layer thickness is

- (A) $\frac{5}{12}$ (B) $\frac{7}{12}$
 (C) $\frac{5}{7}$ (D) $\frac{3}{7}$
5. A Kaplan turbine develops 20000 kW at an average head of 35 m. Assuming a speed ratio of 2, flow ratio of 0.6 and overall efficiency of 90% and taking boss to runner diameter ratio as 0.35, speed of the turbine is
 (A) 365 rpm (B) 388 rpm
 (C) 409 rpm (D) 418 rpm
6. A liquid is flowing between two parallel plates. One plate is moving relative to other with a velocity of 4 m/s in the negative direction. If pressure gradient $\frac{\partial p}{\partial x} = -100 \times 10^6 \text{ N/m}^3$, viscosity $\mu = 0.4$ poise and distance between the plates is 1 m, discharge per meter width is

- (A) 182.5 L/s (B) 190.2 L/s
 (C) 206.8 L/s (D) 242.4 L/s

7. A moving vane with velocity 20 m/s having an inlet angle zero degree and an outlet angle 25° receives water from a jet at a velocity of 48 m/s. Assuming mass flow rate of 1 kg/s, the force acting on the vanes and its inclination is.
 (A) 62.16 N, 15°
 (B) 58.72 N, 13.6°
 (C) 54.68 N, 12.5°
 (D) 50.25 N, 10.4°

8. In the model study of a motor boat in a lake, 1 : 25 scale model is used. It is assumed that viscous resistance due to water and air is negligible compared to the wave resistance. If the speed of the model is 2 m/s, determine the speed of the prototype for dynamically similar conditions
 (A) 8 m/s (B) 10 m/s
 (C) 12 m/s (D) 15 m/s

9. A pipe line through which oil flows has a sudden expansion in it such that maximum pressure rise occurs. Energy loss in the sudden expansion in metres of oil is given by (V_1 = velocity before expansion)

- (A) $\frac{V_1^2}{4g}$ (B) $\frac{V_1^2}{6g}$
 (C) $\frac{V_1^2}{8g}$ (D) $\frac{V_1^2}{2\sqrt{2}g}$

10. Prandtl's velocity distribution for a boundary layer is given by

- (A) $\frac{u}{U} = 2 \left(\frac{y}{\delta} \right) - \left(\frac{y}{\delta} \right)^2$
 (B) $\frac{u}{U} = \frac{3}{2} \left(\frac{y}{\delta} \right) - \frac{1}{2} \left(\frac{y}{\delta} \right)^3$
 (C) $\frac{u}{U} = 2 \left(\frac{y}{\delta} \right) - 2 \left(\frac{y}{\delta} \right)^3 + \left(\frac{y}{\delta} \right)^4$
 (D) $\frac{u}{U} = \sin \left(\frac{\pi y}{2\delta} \right)$

11. Specific speed of a hydraulic pump is the speed of geometrically similar pump working against unit head and
 (A) consuming unit power
 (B) having unit velocity of flow
 (C) having unit radial velocity
 (D) delivering unit quantity of water

ANSWER KEYS

1. B	2. A	3. C	4. A	5. C	6. C	7. C	8. B	9. C	10. B
11. D	12. B	13. D	14. D	15. D	16. C	17. D	18. B	19. D	20. B
21. C	22. B	23. C	24. B	25. B					

HINTS AND EXPLANATIONS

1. The velocity components are

$$u = 3x + 2y$$

$$v = 2z + 3x^2$$

$$w = 2t - 3z$$

Substituting,

$$x = 1, y = 1, z = 1 \text{ and } t = 2$$

$$u = 3 + 2 = 5$$

$$v = 2 + 3 = 5$$

$$w = 2 \times 2 - 3 = 1$$

$$V = \sqrt{u^2 + v^2 + w^2} = \sqrt{5^2 + 5^2 + 1^2} = \sqrt{51}$$

$$= 7.14 \text{ units.}$$

Choice (B)

2. Convective acceleration

$$= v \frac{\partial v}{\partial x} = 2t \left(1 - \frac{x}{2\ell}\right)^2 \times 2t \times 2 \left(1 - \frac{x}{2\ell}\right) \left(-\frac{1}{2\ell}\right)$$

$$= -\frac{4t^2}{\ell} \left(1 - \frac{x}{2\ell}\right)^3$$

Given that $\ell = 1.5 \text{ m}$

$x = 1$ and $t = 5$ seconds

$$\text{convective acceleration} = \frac{-4 \times (5)^2}{1.5} \left(1 - \frac{1}{2 \times 1.5}\right)^3$$

$$= -19.75 \text{ m/s}^2. \quad \text{Choice (A)}$$

3. Total acceleration

= Convective acceleration + local acceleration

$$\text{local acceleration} = \frac{\partial v}{\partial t} = \left(1 - \frac{x}{2\ell}\right)^2 \times 2$$

$$= \left(1 - \frac{1}{2 \times 1.5}\right)^2 \times 2$$

$$= 0.889 \text{ m/s}^2$$

$$\text{Total acceleration} = -19.75 + 0.889 = -18.86 \text{ m/s}^2.$$

Choice (C)

$$4. \frac{u}{U} = \frac{3y}{2\delta} - \frac{1}{2} \frac{y^2}{\delta^2}$$

Displacement thickness

$$\delta^* = \int_0^\delta \left(1 - \frac{u}{U}\right) dy = \int_0^\delta \left(1 - \frac{3y}{2\delta} + \frac{1}{2} \frac{y^2}{\delta^2}\right) dy$$

$$= \left[y - \frac{3}{2} \frac{y^2}{\delta} + \frac{1}{2} \cdot \frac{y^3}{3\delta^2} \right]_0^\delta = \delta - \frac{3}{4} \delta + \frac{\delta}{6} = \frac{5}{12} \delta$$

$$\frac{\delta^*}{\delta} = \frac{5}{12} \frac{\delta}{\delta} = \frac{5}{12}.$$

Choice (A)

$$5. u_1 = k_u \sqrt{2gH} = 2 \sqrt{2 \times 9.81 \times 35} = 52.4 \text{ m/s}$$

$$v_{f1} = k_f \sqrt{2gH} = 0.6 \sqrt{2 \times 9.81 \times 35} = 15.7 \text{ m/s}$$

$$\frac{\text{shaft power}}{wQH} = \text{overall } \eta$$

$$\text{i.e., } \frac{20000 \times 10^3}{9810 \times Q \times 35} = 0.9$$

$$Q = 64.72 \text{ m}^3/\text{s}$$

$$\text{But } Q = \frac{\pi}{4} (D_o^2 - D_b^2) \times v_{f1} \text{ or}$$

$$64.72 = \frac{\pi}{4} D_o^2 (1 - 0.35^2) \times 15.7$$

$$D_o = 2.45 \text{ m}$$

$$u_1 = \frac{\pi D_o N}{60} \text{ where } N = \text{speed of turbine}$$

$$\text{i.e., } 52.4 = \frac{\pi \times 2.45 \times N}{60}$$

$$N = 409.2 \text{ rpm.}$$

Choice (C)

$$6. U = -3 \text{ m/s; } \frac{dp}{dx} = -100 \times 10^6 \text{ N/m}^3$$

$$\mu = 0.4 \text{ poise} = 0.04 \text{ Ns/m}^2$$

$$b = 1 \text{ mm}$$

Discharge per unit width is given by,

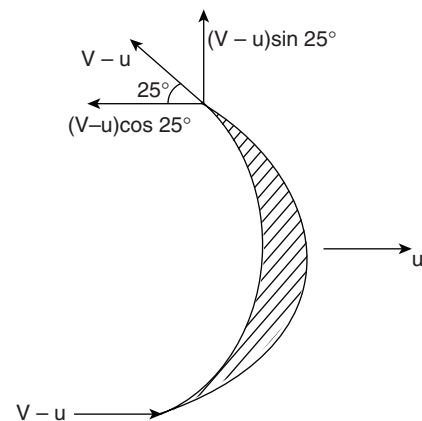
$$q = U \frac{b}{2} - \frac{b^3}{12\mu} \cdot \frac{\partial p}{\partial x}$$

$$= (-3) \times \frac{0.001}{2} - \frac{(0.001)^3}{12 \times 0.04} \times (-100 \times 10^6)$$

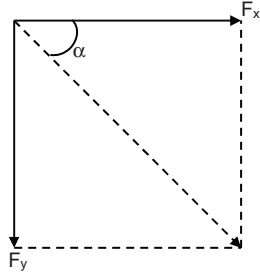
$$= 0.2068 \text{ m}^3/\text{s} = 206.8 \text{ L/s}$$

Choice (C)

- 7.



$$\begin{aligned}
 u &= 20 \text{ m/s} \\
 v_{1x} &= (v - u) = 48 - 20 = 28 \text{ m/s} \\
 v_{1y} &= 0 \\
 v_{2x} &= -(v - u) \cos 25 = -28 \cos 25 = -25.38 \text{ m/s} \\
 v_{2y} &= (v - u) \sin 25 = 28 \sin 25 = 11.83 \text{ m/s} \\
 F_x &= 1 \times [v_{1x} - v_{2x}] = 28 - (-25.38) = 53.38 \text{ m/s} \\
 F_y &= 1 \times [v_{1y} - v_{2y}] = 0 - 11.83 = -11.83 \text{ m/s}
 \end{aligned}$$



Resultant force

$$F_R = \sqrt{F_x^2 + F_y^2} = \sqrt{53.38^2 + (-11.83)^2} = 54.68 \text{ N}$$

$$\tan \alpha = \frac{F_y}{F_x} = \frac{11.83}{53.38} = 0.2216$$

$$\alpha = 12.5^\circ. \quad \text{Choice (C)}$$

8. Since wave resistance is dominant, dynamic similarity will be attained when Froude number is same for model and prototype

$$\text{i.e., } \left(\frac{V}{\sqrt{Lg}} \right)_m = \left(\frac{V}{\sqrt{Lg}} \right)_p \Rightarrow \frac{V_p}{V_m} = \sqrt{\frac{L_p}{L_m}} = \sqrt{25} = 5$$

$$\Rightarrow V_p = 2 \times 5 = 10 \text{ m/s} \quad \text{Choice (B)}$$

9. Maximum pressure rise occurs when $\frac{D_1}{D_2} = \frac{1}{\sqrt{2}}$ or

$$D_2 = \sqrt{2} D_1$$

$$\Rightarrow A_2 = 2A_1 \because A \propto D^2$$

$$\Rightarrow V_2 = \frac{V_1}{2}$$

$$\therefore A_1 V_1 = A_2 V_2 = Q$$

Energy (head) loss in sudden expansion

$$\begin{aligned}
 &= \frac{(V_1 - V_2)^2}{2g} = \frac{\left(V_1 - \frac{V_1}{2} \right)^2}{2g} \\
 &= \frac{V_1^2 \left(1 - \frac{1}{2} \right)^2}{2g} = \frac{V_1^2}{2g} \times \frac{1}{4} = \frac{V_1^2}{8g} \text{ m of oil}
 \end{aligned}$$

Choice (C)

11. Specific speed of hydraulic pump $N_s = \frac{N\sqrt{Q}}{H^{\frac{3}{4}}}$

It is the speed when working against unit head and delivering unit quantity of water. Choice (D)

13. Blades of a propeller turbine are fixed and not adjustable under part load condition. So under part load, water enters with shock and eddies are formed which reduces its efficiency. Choice (D)

15. $P_1 = 1000 \text{ kW}$, $H_1 = 40 \text{ m}$
 $H_2 = 20 \text{ m}$

For both conditions, unit power is same

$$\text{i.e., } P_u = \frac{P_1}{(H_1)^{\frac{3}{2}}} = \frac{P_2}{(H_2)^{\frac{3}{2}}} \Rightarrow P_2 = P_1 \left(\frac{H_2}{H_1} \right)^{\frac{3}{2}}$$

$$\begin{aligned}
 &= 1000 \times \left(\frac{20}{40} \right)^{\frac{3}{2}} = 1000 \times \left(\frac{1}{2} \right)^{\frac{3}{2}} \\
 &= \frac{1000}{\sqrt{8}} \text{ kW}
 \end{aligned}$$

Choice (D)

16. Given- $P_p = 10 \text{ MW}$

$$\frac{D_p}{D_m} = \frac{1}{4}$$

$$\frac{N_p}{N_m} = 1$$

$$\eta_p = \eta_m$$

$$\text{Power coefficient } \frac{P}{N^3 D^5} \text{ is}$$

same in both cases

$$\text{i.e., } \frac{P_p}{N_p^3 D_p^5} = \frac{P_m}{N_m^3 D_m^5}$$

$$\therefore P_m = P_p \times \left(\frac{N_m}{N_p} \right)^3 \times \left(\frac{D_m}{D_p} \right)^5$$

$$= 16 \times 1 \times \left(\frac{1}{4} \right)^5 = \frac{1}{4^3} = \frac{1}{64} \text{ MW}$$

$$= \frac{1000}{64} \text{ kW}$$

Choice (C)

17. Force exerted

$$= \text{mass/second} \times \text{change in velocity of the jet}$$

$$= \rho a v (v - u)$$

Choice (D)

18. $V = C_v \sqrt{2gH}$

$$90 = 0.98 \sqrt{2 \times 9.81 \times H}$$

$$H = 429.87 \text{ m}$$

$$\eta_0 = \frac{P}{wQH} = \frac{7500 \times 10^3}{9810 \times 2.29 \times 429.87} = 0.7766$$

$$Q = \frac{\pi}{4} d^2 \times V$$

$$= \frac{\pi}{4} (0.18)^2 \times 90 = 2.29 \text{ m}^3/\text{s}$$

$$\eta_0 = 0.7766 \times 100 = 77.66 \%$$

Choice (B)

19. Maximum efficiency is expressed as $\eta_H = \frac{1 + \cos \phi}{2}$

$$\phi_1 = 180 - 160 = 20^\circ$$

$$\phi_2 = 180 - 170 = 10^\circ$$

$$\eta_{H1} = \frac{1 + \cos 20^\circ}{2}$$

$$\eta_{H2} = \frac{1 + \cos 10^\circ}{2}$$

$$\frac{\eta_{H1}}{\eta_{H2}} = \frac{(1 + \cos 20^\circ)}{2} \times \frac{2}{1 + \cos 10^\circ}$$

$$= \frac{1.9397}{1.9848} = 0.977$$

Choice (D)

20. $\eta_0 = \frac{P}{wQH}$

$$0.8 = \frac{5520 \times 10^3}{9810 \times Q \times 240}$$

$$Q = 2.931 \text{ m}^3/\text{sec}$$

Unit Discharge

$$Q_u = \frac{Q}{\sqrt{H}} = \frac{2.931}{\sqrt{240}} = 0.189$$

Choice (B)

21. Unit power $Pu = \frac{P}{H^{\frac{3}{2}}} = \frac{5520}{(240)^{\frac{3}{2}}} = 1.485$ Choice (C)

22. $F_n = \rho A V^2 \sin \theta$

$$V = 45 \text{ m/s}$$

$$\theta = 45^\circ = 1000 \times 7.8544 \times 10^{-3} \times (45)^2 \sin 45^\circ$$

$$= 11246 \text{ N}$$

$$F_n = \frac{11246}{1000} = 11.25 \text{ kN}$$

Choice (B)

23. Relative velocity $= v + u = 45 + 15 = 60 \text{ m/s}$

$$F_n = \rho A (v + u)^2 \sin \theta$$

$$= 1000 \times 7.854 \times 10^{-3} (60)^2 \sin 45^\circ$$

$$= 19993 \text{ N}$$

$$F_n = \frac{19993}{1000} = 20 \text{ kN}$$

Choice (C)

24. Net head available at the base of the nozzle

$$= 360 - 12 = 348 \text{ m}$$

$$N_s = \frac{N \sqrt{P}}{H^{\frac{5}{4}}}$$

$$15.33 = \frac{560 \sqrt{P}}{348^{\frac{5}{4}}}$$

$$P = 1686.37 \text{ kW}$$

$$\text{Total power} = 1686.37 \times 3 = 5059.11 \text{ kW} \quad \text{Choice (B)}$$

25. $\eta_0 = \frac{P}{wQH}$

$$0.85 = \frac{1686.37 \times 10^3}{9810 \times Q \times 348}$$

$$Q = 0.581 \text{ m}^3/\text{sec}$$

$$\text{Total discharge} = 3 \times 0.581$$

$$Q = 1.743 \text{ m}^3/\text{s}$$

$$V = k_v \sqrt{2gh} = 0.98 \sqrt{2 \times 9.81 \times 348}$$

$$= 80.98 \text{ m/s}$$

Thus, if the diameter of the nozzle is 'd' then

$$0.581 = \frac{\pi}{4} d^2 \times 80.98$$

$$D = 0.0956 \text{ m} = 95.6 \text{ mm}$$

Choice (B)