

# **Open Channel Flow**

For a wide rectangular channel using Manning's formula, the differential equation of gradually varied flow (with the usual notations) is given by

(a) 
$$\frac{dy}{dx} = S_0 \frac{\left[1 - \left(\frac{y_c}{y}\right)^{10/3}\right]}{\left[1 - \left(\frac{y_0}{y}\right)^3\right]}$$

(b) 
$$\frac{dy}{dx} = S_0 \frac{\left[1 - \left(\frac{y_0}{y}\right)^{10/3}\right]}{\left[1 - \left(\frac{y_0}{y}\right)^3\right]}$$

(c) 
$$\frac{dy}{dx} = S_0 \underbrace{\left[1 - \left(\frac{y_0}{y}\right)^3\right]}_{\left[1 - \left(\frac{y_0}{y}\right)^3\right]}$$

(d) 
$$\frac{dy}{dx} = S_0 \frac{\left[1 - \left(\frac{y_c}{y}\right)^3\right]}{\left[1 - \left(\frac{y_0}{y}\right)^3\right]}$$

- Q.2 Water surface profiles that are asymptotic at one end and terminated at the other end would include
  - (a)  $H_2$  and  $S_2$
- (b)  $H_3$  and  $S_2$
- (c)  $M_2$  and  $H_3$  (d)  $M_1$  and  $H_3$
- Q.3 A hydraulic jump is always needed in case of (a) an A2 profile followed by an A3 profile
  - (b) an A<sub>2</sub> profile followed by an A<sub>3</sub> profile

- (c) an H2 profile followed by an M2 profile
- (d) an M, profile followed by an M, profile
- Consider the following statements in regard to the critical flow:
  - Specific energy is maximum for a given discharge.
  - 2. Specific force is maximum for a given discharge
  - Discharge is maximum for a given specific
  - 4. Discharge is maximum for a given specific

Which of these statements are correct?

- (a) 1, 2, 3 and 4 (b) 1 and 2
- (c) 2 and 3
  - (d) 3 and 4
- Q.5 If  $F_1$  and  $F_2$  are the Froude numbers of flow before and after the hydraulic jump occurring in a rectangular channel, then

(a) 
$$F_2^2 = \frac{F_1^2}{\left(-1 + \sqrt{1 + 8F_1^2}\right)^3}$$

(b) 
$$F_2^2 = \frac{8F_1^2}{\left(-1 + \sqrt{1 + 8F_1^2}\right)^3}$$

(c) 
$$F_2^2 = \frac{F_1^2}{\left(-0.5 + \sqrt{1 + 8F_1^2}\right)^3}$$

(d) 
$$F_2^2 = \frac{8F_1^2}{\left(-0.5 + \sqrt{1 + 8F_1^2}\right)^3}$$

Q.6 Match the following [Column-A (Froude Number) with Column R (Time of budgautic imms))

WILL	1 COMMUNICAD	(IYP	e or r	nyaraulic jump)j
	Column-A	4		Column-B
A.	1.6		1.	Strong jump
В.	2.0		2.	Undullar jump
C.	5.0		3.	Weak jump
Đ.	10.0		4,	Steady jump
Co	des:			
	A B	С	D	

- 3
- Q.7 A hydraulically efficient trapezoidal section of open channel flow carries water at the optimal depth of 0.6 m. Chezy coefficient is 75 and bed slope is 1 in 250. What is the discharge through the channel?
  - (a) 1.44 m<sup>3</sup>/s (b) 1.62 m<sup>3</sup>/s (c)  $1.92 \,\mathrm{m}^3/\mathrm{s}$ (d) 2.24 m<sup>3</sup>/s
- Q.8 Flow depths across a sluice gate are 2.0 m and 0.5 m. What is the discharge (per metre width)?
  - (a) 1.0 m<sup>2</sup>/s
- (b)  $1.4 \,\mathrm{m}^2/\mathrm{s}$
- (c)  $2.0 \text{ m}^2/\text{s}$
- (d)  $2.8 \,\mathrm{m}^2/\mathrm{s}$
- Q.9 Match List-I (Flow section type) with List-II (Critical discharge is proportional to) where y isthe depth of flow and select the correct answer using the codes given below the lists:

	List	-1				List-II
A.	Sha	llow p	arab	olic	1.	$y(z^{1/2})$
₿.	Triar	igulai	ŕ.		2.	y <sup>2/2</sup>
C.	Rec	langu	ılar .		Э.	yE/2
D.	Trap	ezoio	ial -		4.	y2
Co	des:					
	A	В	С	D		
(a)	2	3	4	1		
(b)	4	1	2	3		
(c)	2	ī	4	3		
(d)	4	3	2	1		

Q.10 A hydraulic jump occurs at the top of a spillway. The depth before jump is 0.2 m. The sequent depth is 3.2 m. What is the energy dissipated in in (approximate)?

- (a) 27 (b) 10.5 (c) 15 (d) 42
- Q.11 Most efficient channel section is
  - (a) half hexagon in the form of trapezoid
  - (b) triangular
  - (c) rectangular
  - (d) semicircular
- Q.12 A rectangular channel is 5 m wide and 3 m deep. Water is flowing in the channel for a deoth of 2.5 m. The hydraulic radius is
  - (a) 0.50
- (b) 1.25
- (c) 2.00 (d) None of these
- Q.13 Which one of the following is the correct representation of the sequence of surface profiles if the channel slope changes from mild to steep
  - (a) M. S.
- (b)  $M_1, S_2$
- (c)  $M_2$ ,  $S_2$
- (d) M2, S2
- Q.14 The Chezy's constant C in the Chezy's equation for mean velocity in open channels is
  - (a) is a dimensionless constant
  - (b) has a constant value for different types of channels
  - (c) has dimension L<sup>1/2</sup>T<sup>-1</sup>
  - (d) does not depend on the quality of channel surface
- Q.15 The conveyance Kol a channel is a measure of its carrying capacity. In terms of K, the discharge O is given by
  - (a)  $KC\sqrt{S_0}$
- (b) K. S.
- (c) KAS<sub>0</sub>1/3
- (d) KJRS
- Q.16 The flow characteristic before and after a hydraulic jump are such that:
  - (a) specific forces are equal but specific energies are unequal
  - (b) specific forces are unequal but specific energies are equal
  - (c) neither specific forces nor specific energies
  - (d) specific forces as well as specific energies are equal

Q.17 The ligure below shows a gradually varied flow situation in an open channel with a break in bed slope. Types of water surface profites occurring from left to right are



- (a) H<sub>2</sub>, S<sub>3</sub> (c) ,H<sub>2</sub>, M<sub>3</sub>
- (b) H<sub>2</sub>, S<sub>2</sub> (d) H<sub>3</sub>, M<sub>2</sub>
- Q.18 An open channel carries water with a velocity of 0.605 m/s. If the average bed shear stress is 1.0 N/m2, then the Chezy's constant C is equal
  - ю
  - (a) 500
- (b) 50
- (c) 60
- (d) 6.0
- Q.19 In a subcritical flow, as the specific energy in a channel is decreased, the depth of flow
  - (a) 'also decrease (b) increases
  - (c) does not vary (d) None of these
- Q.20 If the specific energy at the upstream section of a rectangular channel is 3 m and minimum specific energy is 2.5 m, the maximum height of jump without causing afflux will be
  - (a) 0.50 m
- (b) 1.20 m
- (c) 2.50 m
- (d) 5.50 m
- Q.21 The depth of flow for maximum velocity in a circular channel section with diameter equal to 1.5 m is
  - (a) 0.75 m
- (b) 1.065 m
- (c) 1.215 m
- (d) 1.425 m
- Q.22 The critical depth of flow in a most economical triangular channel section for a discharge of 1 m3/sec is given by

(a) 
$$\left(\frac{1}{9.8}\right)^{V5}$$
 metre (b)  $\left(\frac{1}{9.8}\right)^{V3}$  metre

(c) 
$$\left(\frac{1}{4.9}\right)^{VS}$$
 metre (d)  $\left(\frac{1}{4.9}\right)^{VS}$  metre

- Q.23 If the Froude number of flow in a rectangular channel at a depth of flow of yn is For then y Jyn is equal to?
  - (a) F<sub>0</sub><sup>1/3</sup>
- (b) F<sub>0</sub><sup>2/3</sup>
- (c) F<sub>3</sub>/2
- (d)  $F_0^{-1/2}$
- Q.24 If the alternate depths of flow in a rectangular horizontal channel are 0.5 m and 2.0 m respectively then the critical depth of flow will
  - - (b)  $\left(\frac{2}{3}\right)^{V3}$
- (d)  $\left(\frac{4}{5}\right)^{V3}$
- Q.25 Shallow waves in open channels propagate with velocity equal to
  - (a) J2qy
- (b) √gy
- (d)  $\sqrt{y} + \sqrt{\frac{E}{a}}$
- Q.26 Match List-I (Surface profile) with List-II (Description of the profile) and select the correct answer using the codes given below the lists:

List-I List-II

- A. M. 1. Convex upwards; asymptotic horizontal at d/s end: depth increasing with d/s
- B. S. 2. Convex downwards; upstream asymptotic to normal depth with depth decreasing in d/s direction
- 3. Depth increasing downstream and meeting at a angle to CDL; a curve with an inflection point
- D. A. 4. Convex upwards and depth increasing in flow direction: asymptotic to NDL at d/s end

Codes:

- 4 3
- (d) 3 1

∩ 27	io a	uída tantannular	channel if the normal depth			List					
4.2.1			, the percentage increase						cir.	1	
		ie discharge will			1.		-	ariec	TIOW		
					2.		orm f				
		35%	(b) 40%			1.00			d flow		
	(C)	33.3%	(d) 66.7%		4.		_			dy flow	
Q.28	Gra	dually varied flow	in open channel is caused		5.	Spa	tially	varie	d flow		
	whe	-			Co	des:					
	(a)	there is an equil	librium between the forces			Α	В	C	D		
			and those opposing it		(a)	4	3	1	2		
	(b)	~	orces and the change in		(b)	3	4	1	5		
		•	ferent from each other		(c)	4	3	1	5	. 4	
	(c)		ng the flow is not equal to		(d)	4	2	3	5		
	1-,	the resistance to	-								
	M		pe is equal to the normal	Q.33							ed in List-I
4	-,	slope	ps to equal to the nema.					_	_		n in List-II.
		•			Mai	ich Li	st-l (	Desc	ription :	and data)	with List-II
Q.2 <del>9</del>			m deep and has a velocity		(Dis	scharg	geini	m³/s)	and set	ect the corr	ecl answer
	of fix	ow Vis 2.13 m/s.	II a disturbance is caused,		usir	ng the	cod	les gi	ven bel	ow the lists	5:
			can travel upstream with a			List-	-1				
	velo	city of			A.	Rec	angu	ılar ch	annel,	1 mwide, w	ith specific
		1.00 m/s	(b) 2.13 m/s							th = 1,0 m	
	(c)	3.13 m/s	(d) 5.26 m/s		В.					ide slape 1	horizontal:
U 30	Tho	ecosific energy.	E in a critical flow at depth				_			energyato	
4.00			ngular channel is given by			= 1.0		, 41.,(11.	, pour	O Reigy ato	ilioni deba
					^			.lar a	haenal	1 m wide,	اممانات طائب
		$E = 1.25 y_c$	(b) $E = 1.5y_c$		O.		h = 1		ianiei.	i in wice.	With Critical
	(C)	$E = 1.75 y_c$	(d) $E = 2y_c$		_					*	
Q.31	Mos	t economical se	ction of a circular channel		υ.					ving 90° ve	rtex angle
	for	maximum disch	narge should satisfy the					al de	pth = 1	.0 m	
		dition				List-					
	(a)	depth of water =	= 0.95 diameter of circular		1.	1,27				1	
		section			2.	1.71					
	(b)	hydraulic mean	depth = 0.286 diameter of		3.	2.21					
		circular section			4.	3.13					
V	(c)	welled perimeter	r = 2.6 diameters of circular		Co	des:					
	• •	section				A	8	С	D		
	(d)	All of the above			(a)	4	3	2	1		
					(b)	2	1	4	3		
2.32			t-II and select the correct		(c)	2	1	3	4		
	ansy	_	des given below the lists:		(d)	1	2	4	3		
		List-I			• ′		_	·	-		
	A.	Passage of tidal	bore	Q.34	Mai	ch Li	st-l (	Chan	nel sur	lace chara	cteristics)

B. Flow in a river emptying into a lake

D. Flow in a channel with a side weir

C. Flow in a channel at a bend

Q.34 Match List-I (Channel surface characteristics) with List-II (Range of Manning's n) and select the correct answer using the codes given below the lists:

	List-	1									List	41							
A.			chan	nel tr	owell	linish				1.	S,								
В.								clear.		2.	$\tilde{S_2}$								
		ntly (i								3.	M,								
C.					dense	weed	is as	high as		4.	M <sub>2</sub>								:
-		depti								Co	des:								
D.				trea	m-cle	ar loo	se c	obbles,			Α	В	С	D					
	varia	able s	ectio	n						(a)	3	4	2	1					
	List-	-11								(b)	4	3	2	1.					
1.	0.01	<b>6-0</b> .0:	20			,				(c)	3	4	1	2					
2.	0.01	1-0.0	15							(d)	1	3	4	2					
3.	0,03	-0.04									۸	مامند		Seula	ır abaı	anal H	hair	me ita	
	~ ~ .	-0.05							u.s.	' A Z	.umv		recta	Hyur	ir chai	mier II	OMULÉ	ા હા મા	5
4.													-14	0			:caba		
5.	0.10	-0.05 0-0.1													carrie			-	
5.	0.10 des:	0-0.1	25							6.0	m³/s	. If at	a se	ction,	the d	epth	of flav	v is y	5.,
5. Co	0.10 des: A	0-0.1 B	25 C	D						6.0 the	m³/s n ma	. If at	a se ist-l (	ction. Value	the deformation of the office	epth with L	ol (lav List-II	v is y (Type	5 . ∋
5. Co (a)	0.10 des: A 1	0-0.1 B 4	25 C 3	5						6.0 the	m³/s n ma water	. If at tch Li surfa	a se ist-l ( ice p	ction, Value rofile)	the depth of y) and s	epth with L select	ol (lav ist-ll the c	v is y (Type orrec	5 . ∋
5. Co (a) (b)	0.10 des: A 1 2	0-0.1 B 4 4	25 C 3 5	5 5						6.0 the	m <sup>3</sup> /s n ma water swer i	. If at tch Li surfa using	a se ist-l ( ice p	ction, Value rofile)	the depth of y) and so	epth with L select belo	ol (lav ist-ll the c	v is y (Type orrec	5 . ∋
5. Co (a) (b) (c)	0.10 des: A 1 2	0-0.1 B 4 4	25 C 3 5	5 5 3						6.0 the of v	m <sup>3</sup> /s n ma wator swer t List	. If at tch Li surfa using -I	a se ist-l ( ice p	ction, Value rofile) codes	the depth of y) and so given	epth with L select belo	ol (lav ist-ll the c	v is y (Type orrec	5 . ∋
5. Co (a) (b)	0.10 des: A 1 2	0-0.1 B 4 4	25 C 3 5	5 5						6.0 the of vans	m <sup>3</sup> /s n ma wator swer t List 0.63	. If at tch Li surfa using -I 3 m	a se ist-l ( ice p	ction, Value rofile) codes	the depth of y) and signed the control of the contr	epth with L select belo	ol (lav ist-ll the c	v is y (Type orrec	5 . ∋
5. Co (a) (b) (c) (d)	0.10 des: A 1 2 2	0-0.1 B 4 4 1	25 C 3 5 5	5 5 3 4	ain în	nforma	ation	relating		6.0 the of vans	m <sup>3</sup> /s n mai water swer t List 0.63	. If at tch Li surfa using -I 3 m	a se ist-l ( ice p	ction, Value rofile) codes 1. 2.	the de of y) and signed the control of the control	epth with L select belo	ol (lav ist-ll the c	v is y (Type orrec	5 . ∋
5. Co (a) (b) (c) (d)	0.10 des: A 1 2 2 2	0-0.1 B 4 4 1	25 C 3 5 5 3	5 3 4 con				relating ction of		6.0 the of vans	m <sup>3</sup> /s n ma water swer t List 0.63 0.90	. If at tch Li surfa using -I 3 m O m	a se ist-l ( ice p	ction, Value rofile) codes 1. 2. 3.	the depth of the control of the con	epth with L select belo	ol (lav ist-ll the c	v is y (Type orrec	5 . ∋
5. Co (a) (b) (c) (d) Fol	0.10 des: A 1 2 2 2 lowing	0-0.18 4 4 1 1 1 g two	C 3 5 5 3 lists	5 3 4 cont	cient (	chanr	nel se	-		6.0 the of vans	m <sup>3</sup> /s n mai water swer t List 0.63	. If at tch Li surfa using -I 3 m O m	a se ist-l ( ice p	ction, Value rofile) codes 1. 2. 3. 4.	the density in the de	epth with L select belo	ol (lav ist-ll the c	v is y (Type orrec	5 . ∋
5. Co (a) (b) (c) (d) Follotto I dilli	0.10 des: A 1 2 2 lowing he are erent tch Li	O-0.11  B 4 4 1 1 g two shap st-1 (**	C 3 5 3 lists I mos es in Chan	5 3 4 contefficient	cient ns of hape	chanr depth ) with	nel se n of II List-	ction of ow y <sub>om</sub> . II (Area		6.0 the of vans	m <sup>3</sup> /s n ma water swer t 0.63 0.90 1.10	. If at tch Li surfa using -I 3 m O m	a se ist-l ( ice p	ction, Value rofile) codes 1. 2. 3. 4.	the depth of the control of the con	epth with L select belo	ol (lav ist-ll the c	v is y (Type orrec	5 . ∋
5. Co (a) (b) (c) (d) Foliation Ma	0.10 des: A 1 2 2 lowing he are erent tch Li nost e	O-0.1:  B 4 4 1 1 stwo	C 3 5 5 3 lists I mos es in Chan	5 3 4 conteffication	cient ns of hape il sect	chanr depth ) with ion) a	nel se n of II List- ind se	ction of ow y <sub>om</sub> . II (Area elect the		6.0 the of vans	m <sup>3</sup> /s n mai water swer i List 0.60 0.90 1.10 1.40 des:	. If at tch Li surfa using -I 3 m 0 m 0 m	a se ist-l ( ice pi the c	ction, Value rofile) codes 1. 2. 3. 4. 5.	the density in the de	epth with L select belo	ol (lav ist-ll the c	v is y (Type orrec	5 . ∋
5. Co (a) (b) (c) (d) Foliation Ma	0.10 des: A 1 2 2 lowing he are erent tch Li nost e	O-0.1:  B 4 4 1 1 stwo	C 3 5 5 3 lists I mos es in Chan	5 3 4 conteffication	cient ns of hape il sect	chanr depth ) with ion) a	nel se n of II List- ind se	ction of ow y <sub>om</sub> . II (Area		6.0 the of vans	m <sup>3</sup> /s n ma water swer t 0.63 0.90 1.10	. If at tch Li surfa using -I 3 m O m	a se ist-l ( ice p	ction, Value rofile) codes 1. 2. 3. 4.	the density in the de	epth with L select belo	ol (lav ist-ll the c	v is y (Type orrec	5 . ∋

Q.35 Follto th dille Mat of m corr lists:

Codes:

(a) 2

(b) 4

(c) 4

Α В C

> 4 3

> 3 2

> 2 3

Q.36 Match List-I with List-II and select the correct answer using the codes given below the lists:

A. dy/dx is positive and  $y > y_n > y_c$ 

B. dy/dc is negative and  $y_0 > y > y_0$ 

C. dy/dx is negative and  $y_e > y > y_n$ 

D. dy/dx is positive and  $y_c > y_a > y$ 

(d) 1 2 3

List-I

COL	rect answer usir	ng the codes given belo	าเพาใหก		. ~	u
list		ig into occupy given you		(a)	5	3
	List-I	List-II		(b)	5	4
A.	Rectangular	1. 1√3y² <sub>cm</sub>		(c)	3	2
В.	Trapezoidal	2. √3y <sup>2</sup> em		(d)	3	3
C.	Triangle	3. $y_{em}^2$	Q.38	Mat	ch Li	st-lw
		4. 2y <sup>2</sup> <sub>em</sub>		stat	emer	nt :

rith List-II pertaining to the following statement:

2 1

2

2

2

In a channel conveying a discharge O, at section 1, the flow depth is  $y_n$  specific energy is E, and specific force is  $P_1$ . In this channel

List-I

- A. Depth  $y_2$  at which the specific energy is  $E_1$
- B. Depth y, at which the specific force is
- C. Depth y<sub>z</sub> at which the specific energy is
- D. Depth y<sub>s</sub> at which the discharge Q moves with water surface parallel to the bed is
- E. Depth y<sub>0</sub> at the edge of a free fall is

## Lisi-II 1. Brink depth 2. Alternate depth 3. Normal depth 4. Critical depth Conjugate depth Codes: ABC Ď E 3 1 5 2 (b) 5 2 4 3 (c) 1 5 4 3 2 (d) 2 5 4 3 1 Q.39 Match List-I with List-II and select the correct answer using the codes given below the lists: List-I A. Positive surge travelling upstream B. Positive surge travelling downstream C. Negative surge travelling upstream D. Negative surge travelling downstream 1. Occurs on upstream of gate that is partly closed suddenly 2. Occurs on downstream of gate that is partly closed suddenly 3. Occurs on upstream of gate that is opened suddenly 4. Occurs on downstream of gate that is opened suddenly Codes: Α В CD (a) 1 4 3 2 (b) 1 2 3 4 (c) 3 4 1 2 (d) 3 4 2 1

- Q.40 Assertion (A): Any discharge will flow as critical flow in a wide rectangular channel whose bed slope is 1 in  $C^2/q$ .
  - Reason (A): The critical depth of flow through a wide rectangular channel is  $(q^2/g)^{1/3}$ .
  - (a) both A and R are true and R is the correct explanation of A
  - (b) both A and R are true but R is not a correct explanation of A

- (c) A is true but R is false
- (d) A is false but R is true
- Q.41 Consider the following statements:
  - 1. Specific energy increases with the increase in depth of flow.
  - 2. For prismatic channel, the section lactor is a function of the depth of flow,
  - 3. For critical state of flow through a channel, Froude's number should be less than one

Which of these statements is/are correct?

- (a) Both 1 and 3 (b) Only 3
- (c) Both 1 and 2 (d) 1, 2 and 3
- Q.42 Supercritical flow can occur in
  - steep slope profile S.
  - 2. mild slope profile M.
  - 3. critical slope profile C.
  - 4. adverse slope profile A.

Which of these statements are correct?

- (a) 1, 2 and 4
- (b) 1, 2 and 3
- (c) 2,3 and 4
- (d) 1, 2, 3 and 4
- Q.43 Subcritical flow can occur in
  - horizonial slope profile H<sub>2</sub>
  - 2. steep slope profile S,
  - 3. mild slope profile M.
  - 4. critical slope profile C.

Which of these statements is/are correct?

- (a) Only 1
- (b Both 3 and 4
- (c) Both 1 and 3 (d) Both 2 and 3
- Q.44 The given table shows the specific energy of flow (E) at various stages of flow, (d) (both E and d are in meters):
  - 0.6 0.7 0.74 0.8 1.0
  - 1.14 1.11 1.12 12

The unit discharge in this case can be infered as nearly

- (a) 1.25 m<sup>2</sup>/s
- (b) 1.52 m<sup>2</sup>/s
- (c) 2.0 m<sup>2</sup>/s
- (d) 2.08 m<sup>2</sup>/s
- Q.45 Before passage of a surge, the depth and velocity of flow at a section are 1.8 m and 3.72 m/s and after passage, they are 0.6 m and 7.55 m/s respectively. The speed of the surge is
  - (a) + 1.8 m/s
- (b) -2.7 m/s
- (c) +3.6 m/s
- (d) ~4.5 m/s

- Q.46 Which of the following statements are correct?
  - 1. In rigid boundary channels, the shape and roughness factor is not a function of flow parameter.
  - 2. In rigid boundary channels only depth of flow may vary with space and time depending on the nature of flow.
  - 3. The degree of freedom for rigid and mobile boundary channels are 1 and 4 respectively.
  - (a) 1 and 2
- (b) 2 and 3
- (c) 1 and 3
- (d) All of these
- Q.47 Which of the following type of GVF (Gradually Varied Flow) profiles do not exist?
  - (a)  $C_2$ ,  $H_1$ ,  $A_2$
- (b) C2, H2, A1
- (c) C, H, A,
- (d) C., H., A.
- Q.48 Consider the following statements regarding specific energy of flow in an open channel.
  - 1. There is only one specific energy curve for a given channel.
  - 2. Alternate depths are the depths of flow at which the specific energy is same.
  - 3. Critical flow occurs when specific energy is the minimum.

Which of these statements are correct?

- (a) 1 and 2
- (b) 1 and 3
- (c) 2 and 3
- (d) 1, 2 and 3
- Q.49 An irrigation canal has a steady discharge Qat a section where a cross regulator (gate) is provided for control purposes, If the gate of the regulator, which is normally closed is suddenly lifted up to a half-open position, then a rapidly varied unsteady flow results, both upstream and downstream of the gate. In such a case, it would take the form of a
  - (a) +ve surge moving upstream and a -ye surge moving downstream
  - (b) +ve surge moving downstream and a -ve surge moving upstream
  - (c) +ve surge moving upstream and a +ve surge moving downstream
  - (d) -ve surge moving upstream and a -ve surge moving downstream

Q.50 Consider the following statements:

A hydraulic jump occurs in an open channel

- 1. when the Froude number is equal to or less than one.
- 2. at the toe of a spillway.
- downstream of a sluice gate in a canal.
- 4. when the bed slope suddenly changes. Which of these are correct?
- (a) 1, 2, 3 and 4 (b) 1, 2 and 3
- (c) 2, 3 and 4
- (d) 1 and 4
- Q.51 The velocity distribution in a rectangular channel is approximated as  $v = 3.0\sqrt{v}$ . The width of channel is B and depth of flow yn. The kinetic energy correction factor is
  - (a) 1.15
- (b) 1.25
- (c) 1.35
- (d) 1.45
- Q.52 Acircular culvert having diameter 1.0 m is flowing half full and the flow is in critical state. The flow in the culvert barrel is
  - (a) 0.672 m<sup>3</sup>/s
- (b) 0.517 m<sup>3</sup>/s
- (c) 0.771 m<sup>3</sup>/s
- (d) 0.823 m<sup>3</sup>/s
- Q.53 A wide rectangular channel has a longitudinal slope of 0.0004 and its manning's roughness has been assessed as 0.02. The normal depth of this channel when it conveys a discharge intensity of
  - (a) 0.87 m
- (b) 2.13 m
- (c) 1.17 m (d) 1.97 m

1.30 m<sup>3</sup> per sec per metre is

- Q.54 A triangular channel carries a discharge of 3.0 m<sup>3</sup>/sec. It has a vertex angle of 120°. The critical depth for this discharge is
  - (a) 0.821 m
- (b) 0.906 m
- (c) 0.641 m
- (d) 0.986 m

## Comprehension:

A hydraulic jump is formed in a 5 m wide outlet at short distance downstream of the control gate. If the flow depth just downstream of the gate is 2 m and outlet discharge is 150 m<sup>3</sup>/s.

- Q.55 The flow depth downstream of the jump is
  - (a) 11.47 m
- (b) 8.47 m
- (c) 11.63 m
- (d) 8.63 m

## Q.56 The thrust on the gate is

- (a) 2434.5 kN
- (b) 1464.25 kN
- (c) 2812.65 kN
- (d) 2121.60 kN
- Q.57 The velocity distribution in a channel section may be approximated by the equation,  $V = V_0(y/y_0)^n$ in which V is the flow velocity at depth y; V, is flow velocity at depth  $y_n$  and n = a constant. The expression for momentum coefficients is
- (b)  $\frac{(n+1)^3}{3n+1}$

(c) 
$$\frac{(n+1)}{3n+1}$$

(c) 
$$\frac{(n+1)^2}{3(n+1)}$$
 (d)  $\frac{(n+1)^2}{2(n+1)}$ 

Q.58 A 4 m wide rectangular channel is carrying 10 m<sup>3</sup>/sec at depth of 2.5 m. There is step rise of 0.20 m in the channel bottom. Assuming there are no losses at the transition, the flow depth downstream of the bottom step is:

- (a) 2.51 m
- (b) 2,49 m<sub>2</sub>
- (c) 2.48 m
- (d) 2.52 m

#### Answers **Open Channel Flow**

- 2. (c) 3. (d) 4. (d) 5. (b) 6. (d) 7. (b)
- 8. (d)

- 12. (b) 13. (c) 14. (c) 15. (b) 16. (a) 17. (b) 18. (c)
- 22. (c) 23. (b) 24. (d) 25. (b) 26. (a) 27. (c) 28. (c)

- 32. (c) 33. (b) 34. (d) 35. (c) 36. (a) 37. (d) 38. (d)
- 29. (d) . 30. (a) 39. (a) 40. (a)

19. (a) 20. (a)

9. (d)

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10. (b)

- 42. (b) 43. (c) 44. (c) 45. (a) 46. (d) 47. (d) 48. (d)

- 49. (b) 50. (c)
- 51. (c) 52. (c) 53. (c) 54. (b) 55. (d) 56. (a) 57. (d) 58. (b)

#### Explanations Open Channel Flow

1, (b)

$$\frac{dy}{dx} = S_0 \frac{1 - (y_0/y)^N}{1 - (y_0/y)^M}$$

For Chezy's formula N=3: For Manning's formula N = 10/3: M = 3

N is related to conveyance  $\left(\frac{1}{2}AR^{2/3}\right)$ .

The curves which are asymptotic at one end and terminated at the other end are  $M_0$  and  $H_2$ 

From 
$$\frac{dy}{dx} = \frac{S_0 - S_f}{1 - \frac{Q^2T}{gA^3}} = S_0 \frac{1 - \left(\frac{y_0}{y}\right)^{10/3}}{1 - \left(\frac{y_0}{y}\right)^3}$$

Using Manning's equation for wide rectangular

- (i) As  $y \to y_0$ ;  $\frac{dy}{dx} \to 0$  i.e. the water surface approaches normal dooth line
- (ii) As  $y \to y_c$ ;  $\frac{dy}{dx} \to \infty$  i.e. the water surface meets the critical depth line vertically in region 2 and 3.
- (iii) As  $y \to \infty$ ,  $\frac{dy}{dx} \to 0$ ; i.e. the water surface meets a very large depth as horizontal asymptote in region 1.
- (iv) As  $y \to 0$ ,  $\frac{dy}{dx} \to \infty$  it means that the surface profile meets the channel bed vertically in region 3.

- (i)  $M_1$ ,  $M_2$ ,  $S_2$  and  $S_3$  meet  $y_0$  line asymptotically
- (ii) M, and S, curve tend to horizontal as y→∞
- (iii)  $M_0$ ,  $M_3$  and  $S_2$  meet  $\gamma_c$  line normally
- (iv)  $M_2$  and  $S_2$  meet channel bed normally. The slope of:
- C, and C<sub>2</sub> curves comes out to be equal to critical slope of the bed, if Chezy's equation is used. Otherwise they are slightly curved.
- Э. (d)

Hydraulic jump is needed when critical depth line is to be crossed.

(d)

At critical flow, specific energy and specific force is minimum for a given discharge. In other words for a given specific energy or specific force, discharge is maximum at critical flow.

5. (b)

$$\frac{y_2}{y_1} = \frac{\left(-1 + \sqrt{1 + 8F_1^2}\right)}{2} \dots ($$

and 
$$\frac{y_1}{y_2} = \frac{\left(-1 + \sqrt{1 + 8F_2^2}\right)}{2}$$
 ...(ii)

Equating the equation (i) with inverse of equation (ii) we get

$$F_2^2 = \frac{8F_1^2}{\left(-1 + \sqrt{1 + 8F_1^2}\right)^3}$$

$$F_1^2 = \frac{8F_2^2}{\left(-1 + \sqrt{1 + 8F_2^2}\right)^3}$$

(b)

$$Q = CA\sqrt{RS}$$

For hydraulically efficient trapezoidal section.

$$A = \sqrt{3} y_e^2 = \sqrt{3} \times (0.6)^2 = 0.624 \text{ m}$$

$$A = \frac{y_0}{2} = \frac{0.6}{2} = 0.3 \text{ m}$$

$$\therefore Q = 75 \times 0.624 \times \sqrt{0.3 \times \frac{1}{250}} = 1.62 \text{ m}^3/\text{s}$$

(d)

$$\Rightarrow \frac{q^2}{g} = \frac{2\gamma_1^2 \gamma_2^2}{y_1 + y_2}$$

$$\Rightarrow \frac{q^2}{9.81} = \frac{2 \times (2)^2 \times (0.5)^2}{2 + 0.5}$$

$$\Rightarrow q^2 = 0.8 \times 9.81$$

$$\Rightarrow q = 2.8 \text{ m}^2/\text{s}$$

10. (b)

The energy dissipation is given by

$$E_L = \frac{(y_2 - y_1)^3}{4y_1y_2} = \frac{(3.2 - 0.2)^3}{4 \times 0.2 \times 3.2} = 10.55 \text{ m}$$

12. (b)

$$R = \frac{\text{Wetted Area}}{\text{Wetted Perimeter}} = \frac{A}{P}$$
$$= \frac{5 \times 2.5}{5 + 2 \times 2.5} = 1.25$$

14. (c)

Chezy's equation,  $V = C\sqrt{AS}$ Substituting dimensions of each term in above

$$LT^{-1} = C\sqrt{L \times 1}$$

$$C = L^{1/2}T^{-1}$$

15. (b)

Conveyance  $K = \frac{1}{2}AR^{2/3}$ . It expresses the discharge capacity of the channel per unit longitudinal slope

16. (a)

The loss of energy in a hydraulic jump leads to unequal specific energies at downstream and upstream sections.

18. (c)

As we know

$$\tau_0 = \gamma R S_0$$
 ...(i)

$$V = C\sqrt{RS_0}$$

$$\Rightarrow$$
  $V^c = C^c(RS_0)$  ...(ii)  
Dividing (i) by (ii) we get

$$\frac{\tau_0}{V^2} = \frac{\gamma}{C^2}$$

$$\Rightarrow \qquad c^2 = \frac{\gamma V^2}{\tau_0}$$

$$\Rightarrow \qquad c^2 = \frac{9.81 \times 10^3 \times 0.605^2}{1}$$

$$\Rightarrow \qquad c \le 60$$

21. (d) For maximum discharge,  $y = 0.95 \ \tilde{D} = 0.95 \times 1.5$ = 1.425 m

22. (c) We know.

$$\frac{Q^2 I}{gA^3} = 1$$

$$\frac{Q^2 \times 2y_c}{g \times y_c^6} = 1$$

$$y_c^5 = \frac{2Q^2}{g}$$

$$y_c = \left(\frac{2}{9.81}\right)^{1/5} = \left(\frac{1}{4.9}\right)^{1/5}$$

23. (b)  $F_0 = \frac{V}{\sqrt{gy_0}} = \frac{g}{\sqrt{gy_0^3}}$  and  $y_c^3 = g^2/g$ 

$$\therefore \frac{y_c}{y_0} = F_0^{2/3}$$

24. (d)

$$y_1 = 0.5 \text{ m}, y_2 = 20 \text{ m}$$

$$y_0^3 = \frac{2y_1^2y_2^2}{(y_1 + y_2)} = \frac{2 \times \left(\frac{1}{2}\right)^2 \times (2)^2}{\left(2 + \frac{1}{2}\right)}$$

 $y_c = \left(\frac{4}{5}\right)^{1/3}$ 

(a) Specific energy, 26.

$$E = y + \frac{v^2}{2g}$$

For critical flow

$$F = \frac{V}{\sqrt{gD}} = 1$$

$$D = \frac{y}{2}$$
 (for triangular channel)  

$$V^2 = gD$$
  

$$V^2 = \frac{gy}{2}$$
  

$$E = y_c + \frac{gy_c/2}{2} = y_c + \frac{1}{4}y_c$$
  

$$E = \frac{5}{4}y_c = 1.25y_c$$

27. (c)  $Q = AV = (by) \frac{1}{2} y^{2n} s^{nn} = k y^{nn}$  $dQ = \frac{5}{2} k y^{33} dy$  $\frac{dQ}{Q} = \frac{5}{3} \frac{dy}{v} = \frac{5}{2} \times 20\% = 33.3\%$ 

28. (d) If the flow is subcritical, then after the introduction of hump the specific energy will decrease by  $\Delta Z$  (height of hump).

$$E_{c} \le E_{1} - \Delta Z$$

$$\Delta Z \le E_{1} - E_{c}$$

(d) Froude number,

$$F = \frac{V}{\sqrt{gy}} = \frac{2.13}{\sqrt{9.81 \times 1}} = 0.68 < 1$$

Thus, the flow is subcritical

$$C = \sqrt{gy} = \sqrt{9.81 \times 1} = 3.13 \text{ m/s}$$

Upstream velocity

$$= V + C = 2.13 + 3.13 = 5.26 \,\text{m/s}$$

30. (a) Specific energy.

$$E = y + \frac{v^2}{2a}$$

For critical flow,

$$F = \frac{V}{\sqrt{gD}} = 1$$

 $D = \frac{y}{2} \text{ (for triangular channel)}$   $V^2 = gD$ 

$$V^2 = \frac{gy}{gy}$$

$$E = y_c + \frac{gy_c/2}{2}$$

$$E = y_c + \frac{1}{4}y_c$$

$$E = \frac{5}{4}y_c$$

$$E = 1.25y_c$$

(b) 33.

Specific energy,  $E = y = \frac{Q^2}{2\pi \Delta^2}$ For rectangular channel  $y_c = \frac{2}{3}E$ For triangular channel  $y_c = \frac{4}{c}E$ 

37. (d)

$$y_c = \left(\frac{q^2}{g}\right)^{1/3}$$

$$q = \frac{6}{2} = 3 \text{ m}^3/\text{s/m}$$

$$y_c = \left(\frac{3^2}{98}\right)^{1/3} = 0.972 \text{ m}$$

$$y_n = 1.2 \text{ m}$$

 $A \rightarrow y = 0.63 \,\text{m}$   $y_0 = 12 \,\text{m}$   $y_0 = 0.97 \Rightarrow M_3$  $B \rightarrow y = 0.90 \,\text{m}$   $y_n = 12 \,\text{m}$   $y_c = 0.97 \Rightarrow M_3$  $C \rightarrow y = 110 \text{ m}$   $y_n = 12 \text{ m}$   $y_c = 0.97 \Rightarrow M_2$  $D \rightarrow y = 142 \text{ m}$   $y_n = 12 \text{ m}$   $y_n = 0.97 \Rightarrow M_1$ 

40. (a)

For a wide rectangular channel, hydraulic radius R = y (depth of flow) hydraulic depth D = y (depth of flow) For critical flow

$$\frac{V}{\sqrt{gD}} = \frac{V}{\sqrt{gy}} = 1$$

$$\Rightarrow V = \sqrt{gy}$$
From cheav's equation

From chezy's equation

$$V = C\sqrt{RS}$$

$$\Rightarrow V = C\sqrt{yS}$$
From (i) and (ii)

$$S = \frac{1}{G^2 t \sigma}$$

(c) E is min at d = 0.74 m  $1.11 = \frac{V_c^2}{2\sigma} + 0.74$  $V_{-} = 2.69 \, \text{m/s}$  $q = v_x y = 2.69 \times 0.74$ 

46. In rigid boundary channel, only depth of flow may vary with space and time depending on nature of flow. In mobile boundary channels, depth, bed width, bed slope and layout changes with space and time.

 $\simeq 2 \, m^3/s/m$ 

50. (c) Hydraulic jump occurs if super critical flow approaches sub critical flow. Hence statement (1) is wrong, without (1), only option 'c' is correct.

Area of cross-section.

$$A=By_0$$

Average velocity.

$$V = \frac{1}{By_0} \int_0^{y_0} v(Bdy)$$

$$= \frac{1}{y_0} \int_0^{y_0} (3\sqrt{y})Bdy = 3 \times \frac{2}{3}\sqrt{y_0}$$

$$= 2\sqrt{y_0}$$

Kinetic energy correction factor.

$$\alpha = \frac{\int\limits_{0}^{y_{0}} v^{3}(B \, dy)}{B v^{3} y_{0}} = \frac{\int\limits_{0}^{y_{0}} 27 y^{212} B \, dy}{B \left(2 \sqrt{y_{0}^{3}}\right) \times y_{0}}$$

$$\Rightarrow \alpha = \frac{27}{8} \times \frac{y_0^{5/2}}{1} \times \frac{2}{5} \times \frac{1}{y_0^{3/2} \times y_0}$$

$$\Rightarrow \alpha = \frac{27}{20} = 1.35$$

52. (c)

For critical flow,

$$\frac{Q^2}{g} = \frac{A_c^3}{\Gamma_c}$$

For circular conduit flowing half full,

$$A = \frac{\pi D^2}{8} = \frac{\pi (1)^2}{8} = 0.3927 \text{ m}^2$$

Top width,  $T_C = D = 1.0 \text{ m}$ 

Hence,

$$\frac{Q^2}{g} = \frac{A_c^3}{T_c} = \frac{(0.3927)^3}{1.0} = 0.0606$$

- $\Rightarrow Q^2 = 0.0606 \times 9.81 = 0.5941$
- $\Rightarrow$  Q=0.771 m<sup>3</sup>/sec
- 53. (c)

For wide rectangular channel, the hydraulic radius

R=depth of flow y

Using Manning's equation,

Discharge intensity.

$$q = V_y = \frac{1}{2}y^{2/3}S_0^{-1/2} \times y = \frac{1}{2}y^{5/3}S_0^{-1/2}$$

$$1.30 = \frac{1}{0.02} \times y^{5/3} \times (0.0004)^{1/2}$$

$$\Rightarrow y^{5/3} = 1.30$$

54. (b)

$$20 = 120^{\circ}$$

Let  $y_c = critical depth$ 

Top width,

$$T_c = 2y_c \cdot \tan \theta$$

Area,  $A_n = y_n^2 \tan \theta$ 

All critical depth,

$$\frac{Q^2}{g} = \frac{A_c^3}{T_c}$$

$$\Rightarrow \frac{y_c^{5} \tan^3 0}{2y_c \tan \theta} = \frac{1}{2} y_c^{5} \tan^2 \theta$$

$$y_c = \left(\frac{2Q^2}{g} \times \frac{1}{\tan^2 \theta}\right)^{1/5}$$

$$= \left(\frac{2 \times (3)^2}{9.81 \times (\tan 60^\circ)}\right)^{1/5}$$

$$\Rightarrow y_e = 0.906 \,\mathrm{m}$$

55. (d)

Unit discharge,

$$q = \frac{150}{5} = 30 \,\text{m}^3/\text{sec/m}$$

$$V_2 = \frac{q}{y^2} = \frac{30}{2} = 15 \text{ m/sec}$$

$$F_2^2 = \frac{V_2^2}{gy_2} = \frac{(15)^2}{9.81 \times 2} = 11.47$$

Depth downstream of jump

$$y_2 = \frac{y_2}{2} \left( \sqrt{1 + 8F_2^2 - 1} \right) = 8.63 \text{ m}$$

56. (a)

The depth upstream of gate can be determined by applying energy equation between 1 and 2.

$$y_1 + \frac{y_1^2}{2a} = y_2 + \frac{y_2^2}{2a}$$

By substituting the value, we get,

$$y_i = 13.468 \,\mathrm{m}$$

$$P_{I} = F_{s1} - F_{s2}$$

$$= \left(\frac{y_{1}^{2}}{2} + \frac{q^{2}}{gy_{1}}\right) - \left(\frac{y_{2}^{2}}{2} + \frac{q^{2}}{gy_{2}}\right)$$

$$= \left[\frac{(13.68)^{2}}{2} + \frac{(30)^{2}}{9.81 \times 13.468}\right] - \left[\frac{(2)^{2}}{1} + \frac{(30)^{2}}{(9.81 \times 2)}\right]$$

$$= 49.634 \text{ m}^{2}$$
ate =  $YP_{I} \times \text{gate width}$ 

Thruston gate =  $YP_t \times$  gate width = 2434.5 kN

57. (d)

Mean velocity.

$$V_m = \frac{\int v \, dy}{\int dy} = \int_0^{y_0} \frac{V_0 \left(\frac{y}{y_0}\right)^n dy}{\int_0^{y_0} dy}$$

$$= \left[ \frac{V_0 y^{n+1}}{y_0^n \times (n+1)} \right]_0^{y_0} = \frac{V_0}{n+1}$$

$$\beta = \frac{\int_{0}^{y_0} V_0^2 \left(\frac{y}{y_0}\right)^{2n} dy}{\left[\frac{v_0}{(n+1)}\right]_{0}^{2y_0} dy} = \frac{(n+1)^2}{2n+1}$$

58. (b)

$$V_1 = \frac{Q}{A_1} = \frac{10}{4 \times 2.5} = 1 \text{ m/s}$$

$$E_1 = y_1 + \frac{V_1^2}{2g} = 2.5 + \frac{(1)^2}{2 \times 9.81}$$

≃ 2.55 mm

: There are no losses;

$$\Rightarrow E_2 = E_1 - 0.02$$
= 2.55 - 0.2 = 2.35 m

$$\therefore y_2 + \frac{Q^2}{2gA_2^2} = 2.35 \,\text{m}$$

$$y_3^3 - 2.35y_2^2 + 0.32 = 0$$

$$\Rightarrow$$
  $y_2 = 2.29 \text{ m} \Rightarrow (2.29 + 0.20) \text{ m}$ 

Water level d/s of the transition = 2,49 m.